Inductors and Capacitors in the LaPlace Domain

Inductors

From before, the VI characteristics for an inductor are

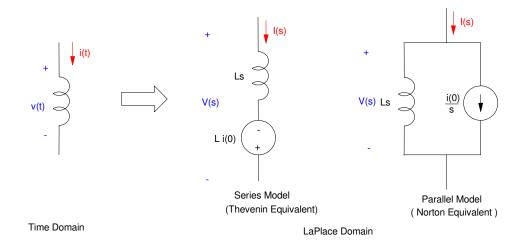
$$v(t) = L\frac{di(t)}{dt}$$

The LaPlace transform is

 $V = L \cdot (sI - i(0))$

Voltages in series add, meaning this is the series connection of two elements: an impedance (Ls) and a voltage source (-Li(0)):

$$V = Ls \cdot I - Li(0)$$



This results in the Thevenin equivalent for an inductor. The Norton equivalent is then

$$I_n = \frac{V_{th}}{R_{th}}$$
$$I_n = \frac{L \cdot i(0)}{Ls}$$
$$I_n = \frac{i(0)}{s}$$

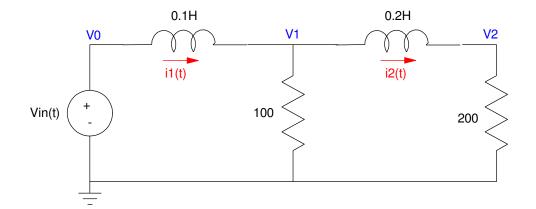
Note that

- The series model is more useful when writing current loop equations
- The parallel model is more useful when writing voltage node equations.

Both models are valid, however.

Example 1: Determine the voltages for the following circuit. Assume

$$v_{in}(t) = \begin{cases} 5V & t < 0\\ 10V & t > 0 \end{cases}$$



Solution: First, find the currents at t = 0. Using phasor analysis, the inductors become

$$L \to j\omega L = 0$$

For t<0, this results in

$$v_{1} = v_{2} = 5V$$

$$i_{2} = \frac{5V}{200\Omega} = 25mA$$

$$i_{1} = \frac{5V}{100\Omega} + i_{2} = 75mA$$

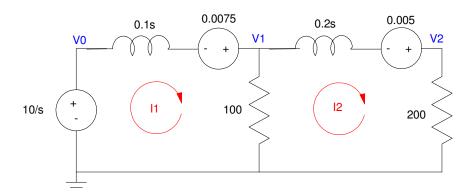
Now, take the LaPlace transform. Assuming we're going to be using current loops, use the series model for the inductors.

$$v_{in} \rightarrow \frac{10}{s}$$

$$0.1H \rightarrow 0.1s - 0.1 \cdot i_1(0)$$

$$\rightarrow 0.1s - 0.0075$$

$$0.2H \rightarrow 0.2s - 0.2 \cdot i_2(0)$$
$$\rightarrow 0.2s - 0.005$$

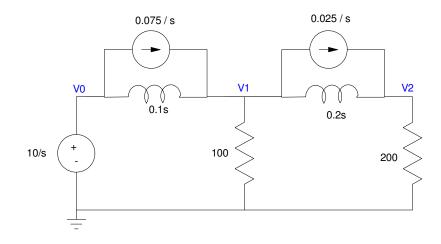


Writing the current loop equations:

$$-\frac{10}{s} + 0.1s \cdot I_1 - 0.0075 + 100(I_1 - I_2) = 0$$

$$100 \cdot (I_2 - I_1) + 0.2s \cdot I_2 - 0.005 + 200 \cdot I_2 = 0$$

The parallel model (for voltage nodes) would be



with the voltage node equations being

$$V_{0} = \frac{10}{s}$$

$$\left(\frac{V_{1} - V_{0}}{0.1s}\right) - \left(\frac{0.075}{s}\right) + \left(\frac{V_{1}}{100}\right) + \left(\frac{0.025}{s}\right) + \left(\frac{V_{1} - V_{2}}{0.2s}\right) = 0$$

$$\left(\frac{V_{2} - V_{1}}{0.2s}\right) + \left(\frac{V_{2}}{200}\right) - \left(\frac{0.025}{s}\right) = 0$$

Capacitors

From before, the VI characteristics for a capacitor is

$$i(t) = C\frac{dv}{dt}$$

Taking the LaPlace transform

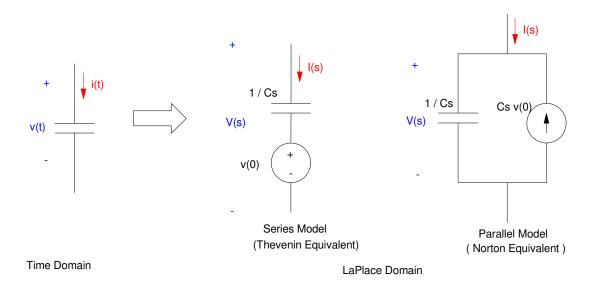
$$I(s) = C \cdot (sV - v(0))$$
$$I(s) = CsV - Cv(0)$$

Solving for V

$$V = \left(\frac{1}{Cs}\right)I + v(0)$$

This gives the series (Thevenin) model for a capacitor. The parallel model has

$$I_{short} = \frac{V_{th}}{R_{th}} = \frac{v(0)}{1/Cs} = Csv(0)$$



Note that

- The series model is more useful when writing current loop equations
- The parallel model is more useful when writing voltage node equations.

Example: Convert the following circuit to the LaPlace domain and write the voltage node and current loop equations.

$$v_{in}(t) = \begin{cases} 5V & t < 0\\ 10V & t > 0 \end{cases}$$

$$v_{in}(t) = \begin{cases} 5V & t < 0\\ 10V & t > 0 \end{cases}$$

$$v_{in}(t) = \begin{cases} 0.01F & 0.02F \\ 0.01F & 0.$$

Solution: First find the initial conditions. For t<0, the voltage is a constant (5V). Using phasor analysis,

$$C \to \frac{1}{j\omega C} = \infty$$
$$V_1 = V_2 = 5V$$

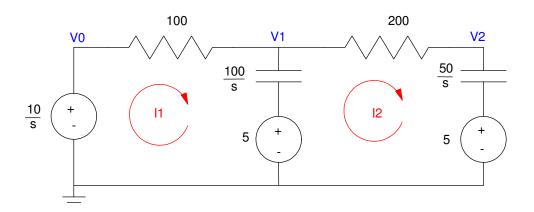
For the series (Thevenin) model, you have a voltage source with

$$V_{th} = v(0) = 5$$

For the parallel (Norton) model, you have a current source with

$$I_N = \frac{V_{th}}{R_{th}} = \frac{v(0)}{1/Cs} = C \cdot v(0) \cdot s$$

Series Model for t > 0:

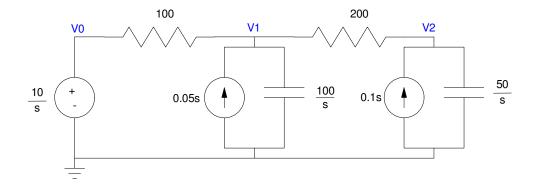


The current loop equations are then:

$$-\frac{10}{s} + 100I_1 + \left(\frac{100}{s}\right)(I_1 - I_2) + 5 = 0$$

$$-5 + \left(\frac{100}{s}\right)(I_2 - I_1) + 200I_2 + \left(\frac{50}{s}\right)I_2 + 5 = 0$$

Parallel Model for t > 0:



the voltage node equations become

$$V_0 = \frac{10}{s}$$

$$\left(\frac{V_1 - V_0}{100}\right) - 0.05s + \left(\frac{V_1}{100/s}\right) + \left(\frac{V_1 - V_2}{200}\right) = 0$$

$$\left(\frac{V_2 - V_1}{200}\right) - 0.1s + \left(\frac{V_2}{50/s}\right) = 0$$