

# ECE 321 - Solutions to the Final

Spring 2018

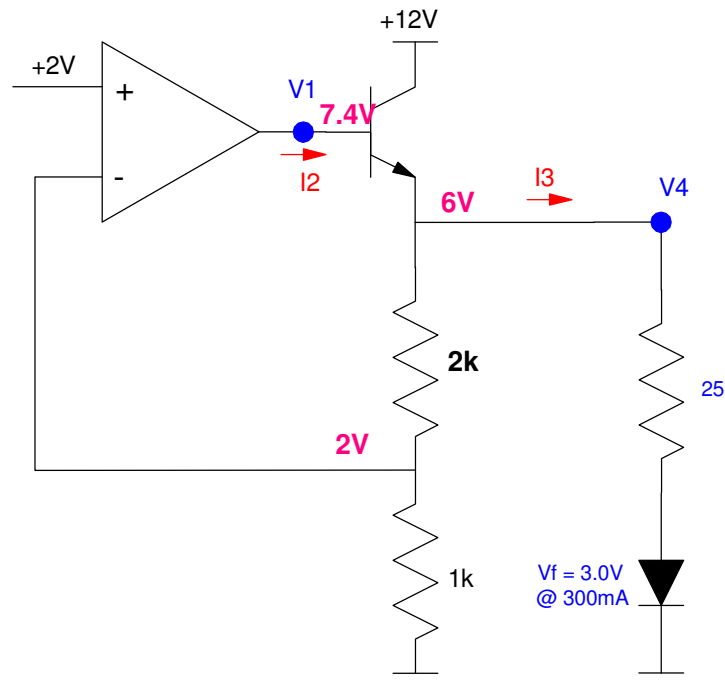
1) Determine the voltages and currents for the following push (pull) amplifier. Assume for the transistor

- $\beta = 1000$
- $V_{be} = 1.4V$

Assume for the LED

- $V_f = 3.0V @ 300mA$ :

V1	I2	I3	V4
<b>7.4V</b>	<b>124.9<math>\mu</math>A</b>	<b>120mA</b>	<b>6V</b>



$V_+$  equals  $V_-$ . This means  $V_4$  must be 6V for  $V_-$  to be +2V

$$V_1 = V_4 + 1.4V \quad (V_{be}) = 7.4V$$

$$I_3 = \left( \frac{6V - 3.0V}{25\Omega} \right) = 120mA$$

$$I_e = I_3 + \frac{6V}{3k} = 125mA$$

$$I_b = \frac{I_e}{1+\beta} = \frac{125mA}{1001} = 124.9\mu A$$

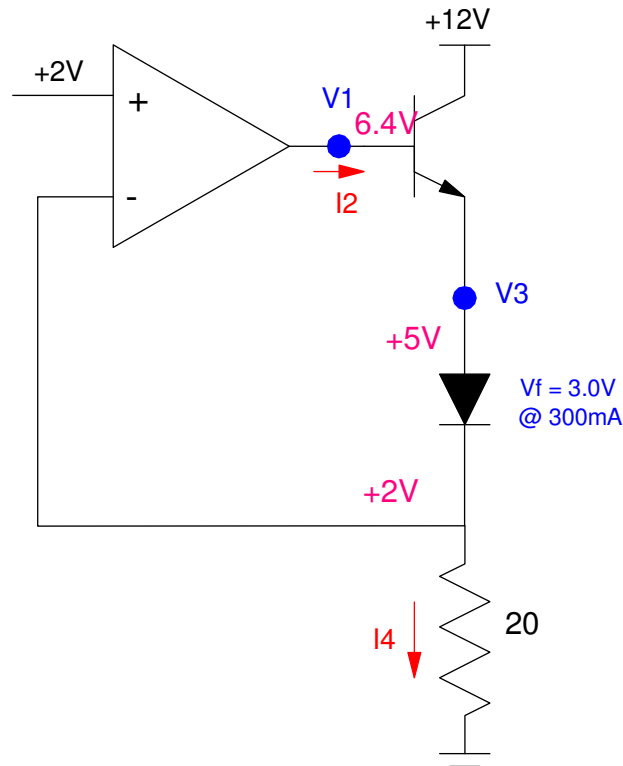
2) Determine the voltages and currents for the following push (pull) amplifier. Assume for the transistor

- $\beta = 1000$
- $V_{be} = 1.4V$

Assume for the LED

- $V_f = 3.0V @ 300mA$ :

V1	I2	V3	I4
<b>6.4V</b>	<b>99.9<math>\mu</math>A</b>	<b>5.0V</b>	<b>100mA</b>



$$V_+ = V_- = 2V$$

$$I_4 = \frac{2V}{20\Omega} = 100mA$$

$$V_3 = 2V + 3V = 5V$$

$$I_2 = I_b = \frac{I_e}{1+\beta} = \frac{100mA}{1001} = 99.9\mu A$$

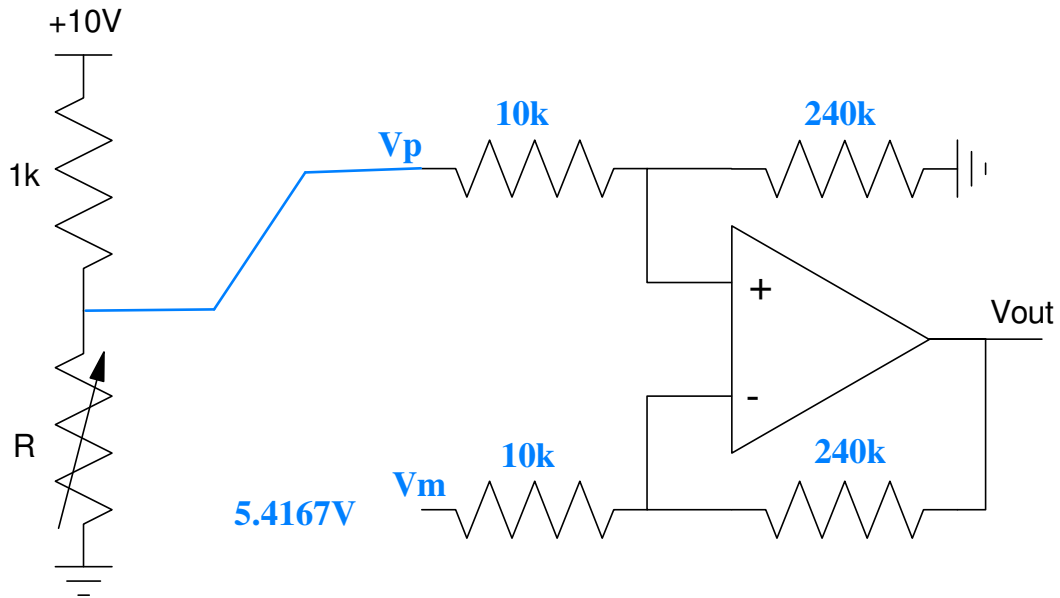
$$V_1 = V_3 + V_{be} = 6.4V$$

3) Design an instrumentation amplifier so that the output is

- -10V when R = 1000 Ohms
- +10V when R = 1400 Ohms

For your circuit, what is the output voltage (Vout) when R = 1100 Ohms?

Vout when R = 1100: **Vout = -4.2865V**



R = 1000 Ohms (Vo = -10V)

$$V_a = \left( \frac{R}{R+1000} \right) 10V = 5.00V$$

R = 1400 Ohms (Vo = +10V)

$$V_a = \left( \frac{R}{R+1000} \right) 10V = 5.833V$$

Gain:

$$gain = \left( \frac{10V - (-10V)}{5.833V - 5.000V} \right) = 24.0$$

The output goes up as the input get larger. Connect to the plus input

$$Y = gain(V_p - V_m)$$

$$+10V = 24.0(5.833V - V_m)$$

$$V_m = 5.4167V$$

At 1100 Ohms

$$V_p \approx \left( \frac{R}{R+1000} \right) \cdot 10V = 5.2381V$$

$$Y = 24(5.2183 - 5.4167) = -4.2865V$$

4) Give the transfer function for a low-pass filter which comes close to meeting the following requirements

- $0.9 < \text{Gain} < 1.1$  frequencies less than 500 rad/sec
- $\text{Gain} < 0.2$  frequencies above 600 rad/sec

You are free to choose any type of filter you like (Chebychev, Butterworth, Elliptic, etc.)

The number of poles you need are

$$\left(\frac{500\text{Hz}}{600\text{Hz}}\right)^N = 0.2$$

$$N = 8.82$$

Round up to  $N = 9$

Assume a Butterworth filter. For 9 poles, the angle between poles is

$$\theta = \left(\frac{180^\circ}{N}\right) = 20^\circ$$

Place the corner at 500 rad/sec (may need to adjust with Matlab)

Make the numerator whatever it takes so that the DC gain is 1.000

$$G(s) = \left( \frac{500^9}{(s+500)(s+500\angle\pm 20^\circ)(s+500\angle\pm 40^\circ)(s+500\angle\pm 60^\circ)(s+500\angle\pm 80^\circ)} \right)$$

5) A 3rd-order Butterworth low-pass filter has the following transfer function:

$$Y = \left( \frac{250}{(s+5)(s^2+5s+25)} \right) X = \left( \frac{250}{s^3+10s^2+50s+125} \right) X$$

a) What is the differential equation relating X and Y?

$$(s^3 + 10s^2 + 50s + 125)Y = 250X$$

'sY' means 'the derivative of Y'

$$y''' + 10y'' + 50y' + 125y = 250x$$

b) Determine y(t) assuming

$$x(t) = 3 \sin(7t) + 5 \cos(8t)$$

Use super position

$$x(t) = 3 \sin(7t)$$

$$X = 0 - j3$$

$$s = j7$$

$$\left( \frac{250}{s^3+10s^2+50s+125} \right)_{s=j7} = 1.8492 \angle -3.30^\circ$$

$$Y = (1.8492 \angle -3.30^\circ)(0 - j3)$$

$$Y = 5.5476 \angle -93.30^\circ$$

$$y(t) = 5.5476 \cos(7t - 93.30^\circ)$$

$$x(t) = 5 \cos(8t)$$

$$X = 5 + j0$$

$$s = j8$$

$$\left( \frac{250}{s^3+10s^2+50s+125} \right)_{s=j8} = 1.1849 \angle 32.03^\circ$$

$$Y = (1.1849 \angle 32.03^\circ)(5 + j0)$$

$$Y = 5.9199 \angle 32.03^\circ$$

$$y(t) = 5.9199 \cos(8t + 32.03^\circ)$$

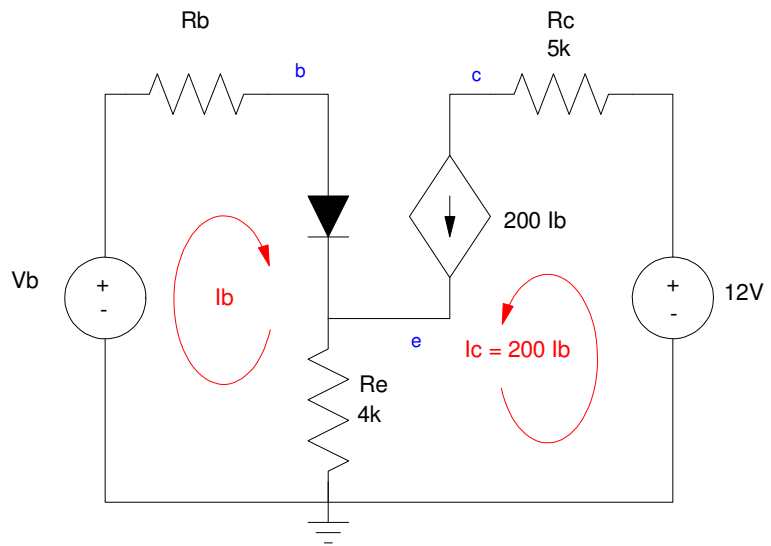
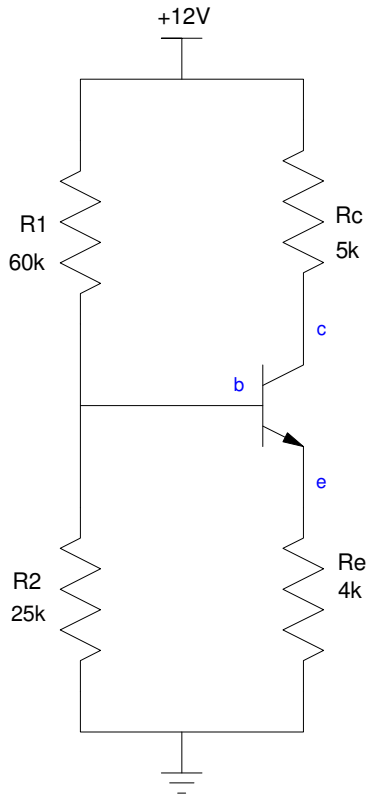
The total answer is the sum of the two parts:

$$y(t) = 5.5476 \cos(7t - 93.30^\circ) + 5.9199 \cos(8t + 32.03^\circ)$$

6) Find the Thevenin equivalent of R1, R2 (Vb, Rb), and the Q-point (Ic, Vce) for the following transistor circuit. Assume a 3904 transistor:

- $\beta = 200$
- $V_{be} = 0.7V$

Vb	Rb	Ic	Vce
<b>3.5294V</b>	<b>17,657</b>	<b>688.7<math>\mu</math>A</b>	<b>5.788V</b>



$$R_b = R_1 || R_2 = 17,647\Omega$$

$$V_b = \left( \frac{R_2}{R_1 + R_2} \right) 12V = 3.5294V$$

$$I_b = \left( \frac{V_b - 0.7V}{R_b + (1 + \beta)R_e} \right) = 3.4436\mu A$$

$$I_c = \beta I_b = 688.7\mu A$$

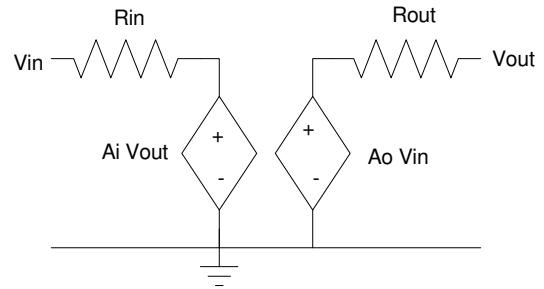
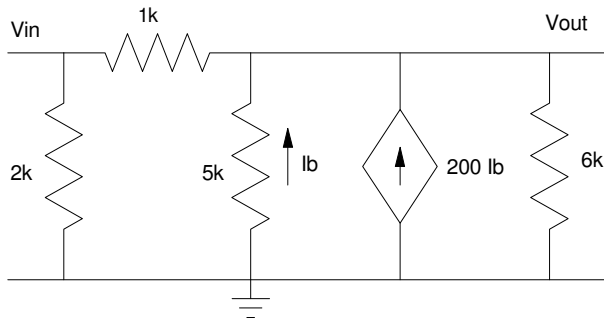
$$V_e = R_e (I_b + I_c) = 2.769V$$

$$V_c = 12 - 5000 I_c = 8.556V$$

$$V_{ce} = V_c - V_e = 5.788V$$

7) Find the 2-port model for the following circuit:

Rin	Ai	Rout	Ao
<b>667 Ohms</b>	<b>0.667</b>	<b>186.3 Ohms</b>	<b>0.02417</b>



Rin: Short Vout. Apply 1V to Vin. Compute Rin.

$$R_{in} = 2k \parallel 1k = 667\Omega$$

Ai: Apply 1V tgo Vout. Measure Vin

$$A_i = \left( \frac{2k}{2k+1k} \right) 1V = 0.667V$$

Rout: Short Vin. Apply 1V to Vout. Comptue the current draw

$$I = \left( \frac{1V}{1k} \right) + \left( \frac{1V}{5k} \right) + 200 \left( \frac{1V}{5k} \right) + \left( \frac{1V}{6k} \right) = 5.367mA$$

$$R_{out} = \left( \frac{1V}{5.367mA} \right) = 186.3\Omega$$

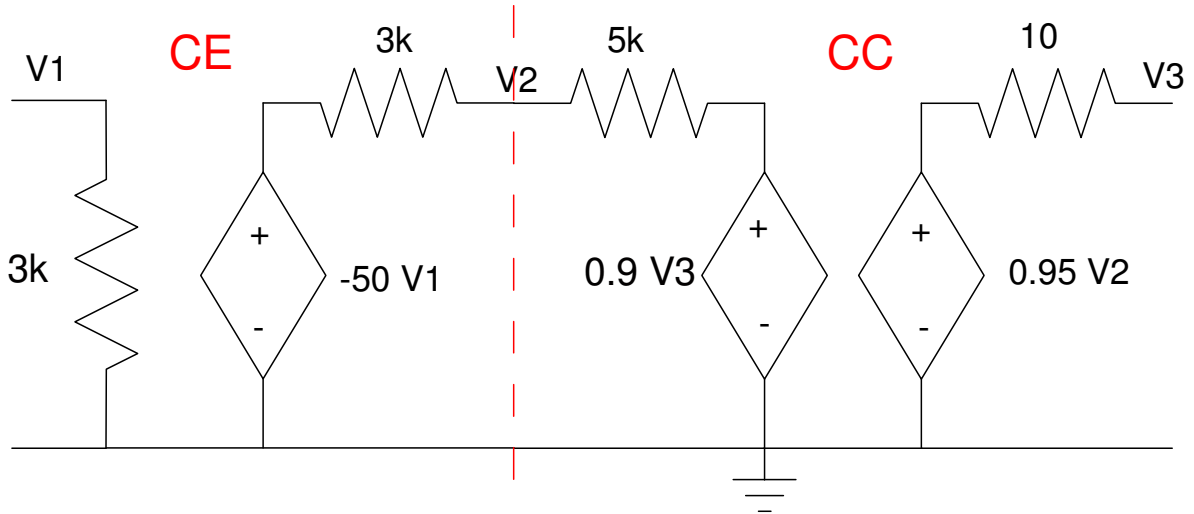
Ao: Apply 1V to Vin. Compute Vout

$$\left( \frac{V_{out}-1}{1k} \right) + \left( \frac{V_{out}}{5000} \right) + 200 \left( \frac{V_{out}}{5000} \right) + \left( \frac{V_{out}}{6000} \right) = 0$$

$$V_{out} = 0.02417$$

8) Find the 2-port model for the following CE : CC amplifier

Rin	Ai	Rout	Ao
<b>3k</b>	<b>0</b>	<b>14.72 Ohms</b>	<b>-43.70</b>



Rout: Short V1. Apply 1V to V3. Compute the current

$$V_2 = \left( \frac{3k}{3k+5k} \right) \cdot 0.9 = 0.3375V$$

$$I = \left( \frac{1V - 0.95 \cdot 0.3375V}{10\Omega} \right) = 67.94mA$$

$$R_{out} = \frac{1V}{67.94mA} = 14.72\Omega$$

Ao: Apply 1V to Vin. Compute V3

$$V_2 = \left( \frac{5k}{3k+5k} \right) (-50V) + \left( \frac{3k}{3k+5k} \right) (0.9V_3)$$

$$V_3 = 0.95V_2$$

$$V_2 = -46.00V$$

$$V_3 = 0.95V_2 = -43.70V$$



