

System Modeling and State-Space

There are several ways to express a dynamic system. In ECE 343, you used transfer functions, such as

$$Y = \left(\frac{10}{s^2 + 2s + 10} \right) X$$

In this class, we'll be using a formulation called State Space. State-space is an energy-based system to describe the dynamics of a system. In essence, the states, X , define the energy in the system. The change in the energy describes how the system behaves as

$$sX = AX + BU$$

What you measure is also a function of the energy in the system.

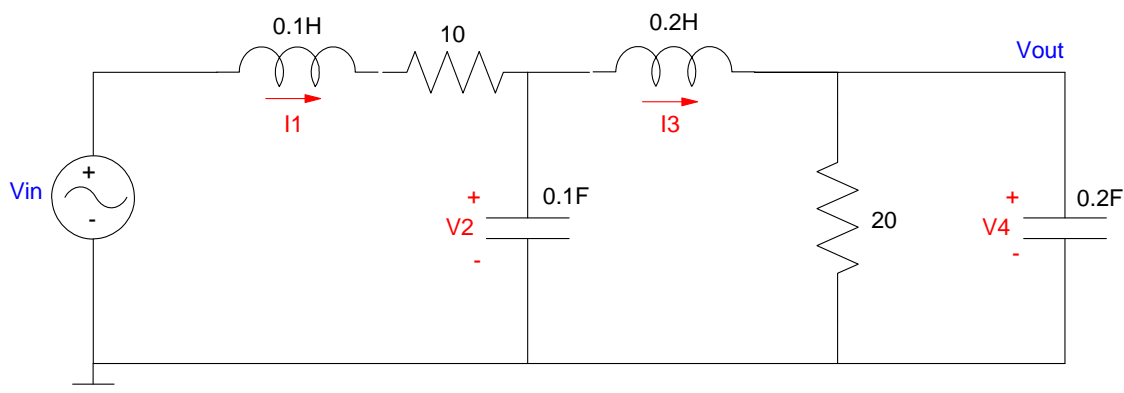
$$Y = CX + DU$$

Together, this gives you a state-space representation for a system:

Example 1: RLC Circuit

For the following RLC circuit,

- Find the transfer function for the following circuit from V_{in} to V_{out}
- Find the dominant pole of this system
- Determine a 1st or 2nd-order approximation for this system:



Example 1: RLC Circuit

Let the states, X , define the energy in the system (the current through the inductors and the voltage across the capacitors):

$$X = \begin{bmatrix} I_1 \\ V_2 \\ I_3 \\ V_4 \end{bmatrix}$$

The change in the states can then be found using the basic equations for an inductor and capacitor:

$$V = L \frac{dI}{dt}$$

$$I = C \frac{dV}{dt}$$

The voltage across the first inductor is then

$$V_{L1} = 0.1sI_1 = V_{in} - (V_2 + 10I_1)$$

The current to capacitor 2 is

$$I_{C2} = 0.1sV_2 = I_1 - I_3$$

The voltage across inductor 3 is

$$V_{L3} = 0.2sI_3 = V_2 - V_4$$

The current to capacitor 4 is

$$I_{C4} = 0.2sV_4 = I_3 - \frac{V_4}{20}$$

Put these together and you get

$$sI_1 = 10V_{in} - 10V_2 - 100I_1$$

$$sV_2 = 10I_1 - 10I_3$$

$$sI_3 = 5V_2 - 5V_4$$

$$sV_4 = 5I_3 - 0.25V_4$$

In matrix form (a.k.a. state-space form):

$$\begin{bmatrix} sI_1 \\ sV_2 \\ sI_3 \\ sV_4 \end{bmatrix} = \begin{bmatrix} -100 & -10 & 0 & 0 \\ 10 & 0 & -10 & 0 \\ 0 & 5 & 0 & -5 \\ 0 & 0 & 5 & -0.25 \end{bmatrix} \begin{bmatrix} I_1 \\ V_2 \\ I_3 \\ V_4 \end{bmatrix} + \begin{bmatrix} 10 \\ 0 \\ 0 \\ 0 \end{bmatrix} V_{in}$$

The output is equal to V_4 , so

$$V_{out} = \begin{bmatrix} 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} I_1 \\ V_2 \\ I_3 \\ V_4 \end{bmatrix} + [0]V_{in}$$

In Matlab, you can find the transfer function:

```
>> A = [-100,-10,0,0;10,0,-10,0;0,5,0,-5;0,0,5,-0.25]
-100.0000 -10.0000 0 0
 10.0000 0 -10.0000 0
 0 5.0000 0 -5.0000
 0 0 5.0000 -0.2500

>> B = [10;0;0;0]
10
0
0
0

>> C = [0,0,0,1]
0 0 0 1

>> D = 0
0

>> G4 = ss(A,B,C,D);
```

The transfer function from V_{in} to V_{out} is:

```
>> zpk(G4)
-----
          2500
(s+98.99) (s+0.5025) (s^2 + 0.7525s + 75.38)
```

Its first-order approximation is:

- A 1st-order system
- With a DC gain of 0.6667, and
- A 2% settling time of 8 seconds ($4 / 0.5025$).

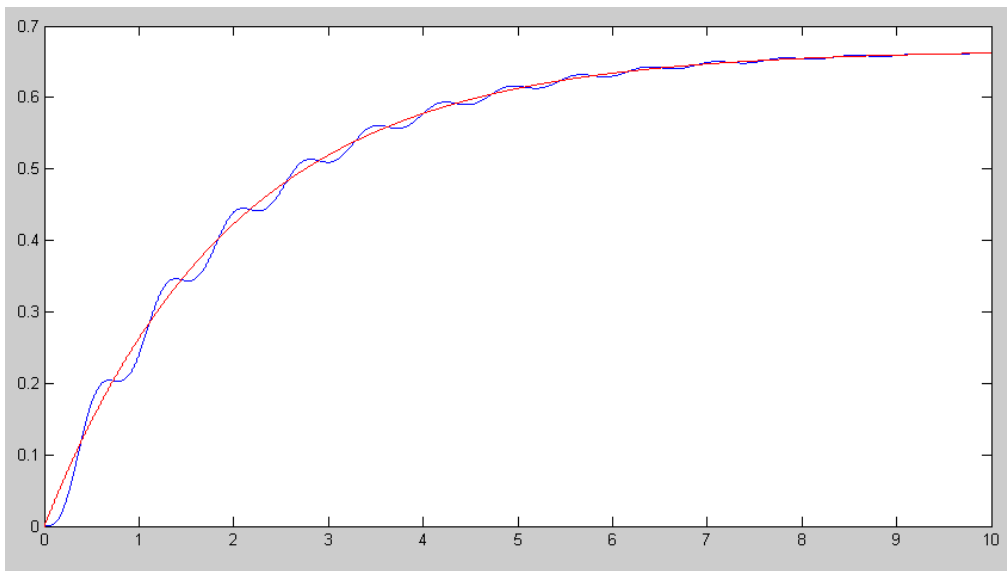
```
>> DC = evalfr(G4,0)
0.6667

>> G1 = tf(0.6667*0.5025,[1,0.5025])

0.335
-----
s + 0.5025

>> y4 = step(G4,t);
>> y1 = step(G1,t);
>> plot(t,y4,'b',t,y1,'r');
```

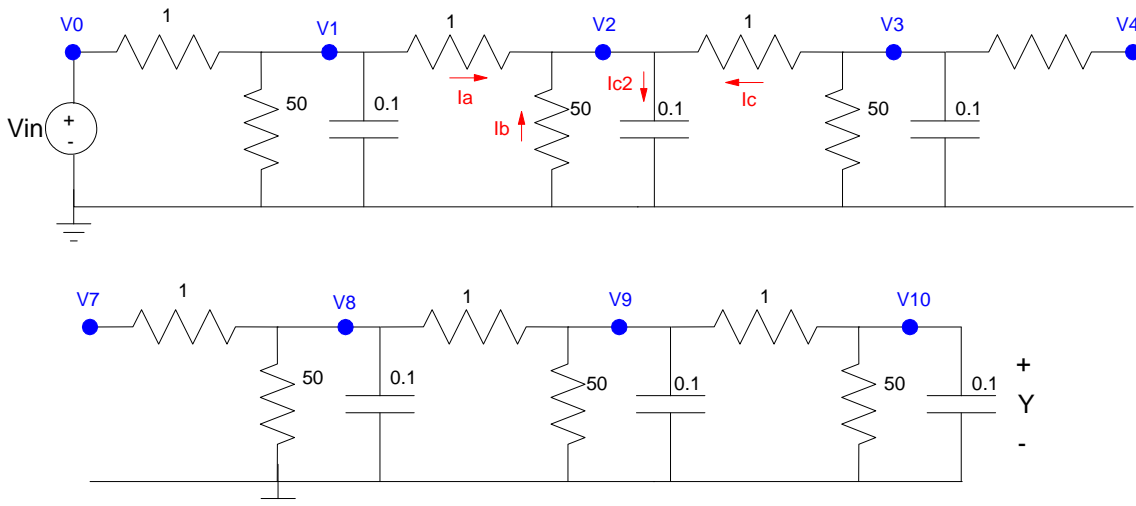
The actual step response from Matlab is as follows:



Step Response of the 4th-order RLC circuit (blue) and its 1st-order approximation (red)

Example 2: RC Filter (Heat Equation)

Consider next the following 10-stage RC filter



Example 2: 10-stage RC filter

While this looks daunting, in state-space it isn't that bad. Since each stage is identical, the equations will be the same. Take node 2 for example. The current to the capacitor (I_{C2}) is the sum of the currents coming in:

$$I_{C2} = I_a + I_b + I_c$$

$$I_{c2} = CsV_2 = \left(\frac{V_1 - V_2}{1} \right) + \left(\frac{0 - V_2}{50} \right) + \left(\frac{V_3 - V_2}{1} \right)$$

or

$$sV_2 = 10V_1 - 20.2V_2 + 10V_3$$

This repeats for nodes 1..9. Node #10 is slightly different since it only connects to one other node::

$$I_{c10} = CsV_{10} = \left(\frac{V_9 - V_{10}}{1} \right) + \left(\frac{0 - V_{10}}{50} \right)$$

$$sV_{10} = 10V_9 - 10.2V_{10}$$

In Matlab:

```
>> A = zeros(10,10);
>> for i=1:9
    A(i,i) = -20.2;
    A(i,i+1) = 10;
    A(i+1,i) = 10;
end
>> A(10,10) = -10.2;

-20.2000  10.0000   0         0         0         0         0         0         0         0
 10.0000 -20.2000  10.0000   0         0         0         0         0         0         0
 0        10.0000 -20.2000  10.0000   0         0         0         0         0         0
 0         0       10.0000 -20.2000  10.0000   0         0         0         0         0
 0         0         0       10.0000 -20.2000  10.0000   0         0         0         0
 0         0         0         0       10.0000 -20.2000  10.0000   0         0         0
 0         0         0         0         0       10.0000 -20.2000  10.0000   0         0
 0         0         0         0         0         0       10.0000 -20.2000  10.0000   0
 0         0         0         0         0         0         0       10.0000 -20.2000  10.0000
 0         0         0         0         0         0         0         0       10.0000 -10.2000
 0         0         0         0         0         0         0         0         0       10.0000

>> B = [10;0;0;0;0;0;0;0;0;0]

 10
  0
  0
  0
  0
  0
  0
  0
  0
  0

>> C = [0,0,0,0,0,0,0,0,0,1];
>> D = [0];
>> G = ss(A,B,C,D);
>> evalfr(G,0)

    0.4325

>> zpk(G)

-----
10000000000
-----
(s+39.31) (s+36.72) (s+32.67) (s+27.51) (s+21.69) (s+15.75) (s+10.2) (s+5.539) (s+2.181) (s+0.4234)
```

This is the transfer function for this RC filter. Its response should

- Have a DC gain of 0.4325, and
- A 2% settling time of 9.44 seconds ($4 / 0.4234$)

$$G(s) \approx \left(\frac{0.1793}{s+0.4234} \right)$$

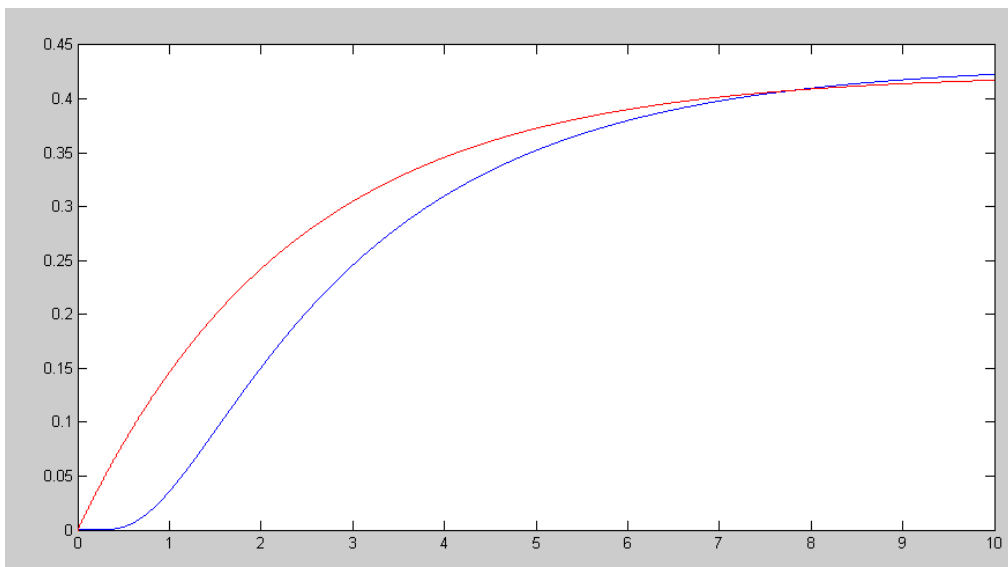
The actual step-response from Matlab is

```
>> G1 = zpk([],[-0.4234],0.1793)

Zero/pole/gain:
  0.1793
-----
(s+0.4234)

>> t = [0:0.001:10]';
>> y1 = step(G1,t);
>> y10 = step(G10,t);
??? Undefined function or variable 'G10'.

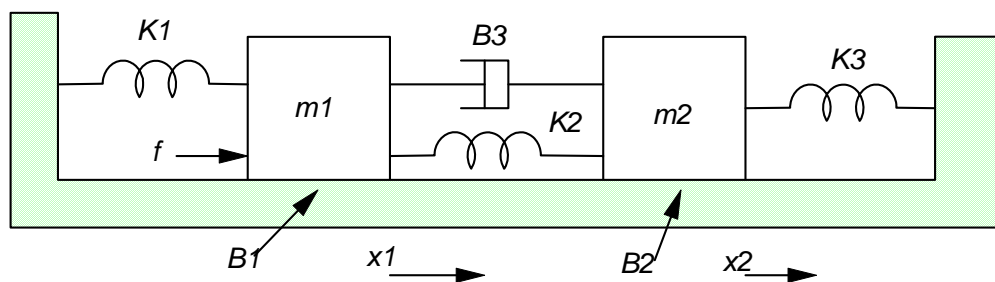
>>
>> y10 = step(G,t);
>> plot(t,y10,'b',t,y1,'r');
```



Step Response of the 10th Order RC Filter (blue) and its 1st-Order Approximation (red)

Example 3: Mass-Spring System

Finally, consider a mass-spring system:



Example 3: Mass Spring System

To put this in state-space form, redraw this as a circuit equivalent using the following dual:

$$I = \frac{1}{R} \cdot V$$

$$F = Ms^2 \cdot X$$

If

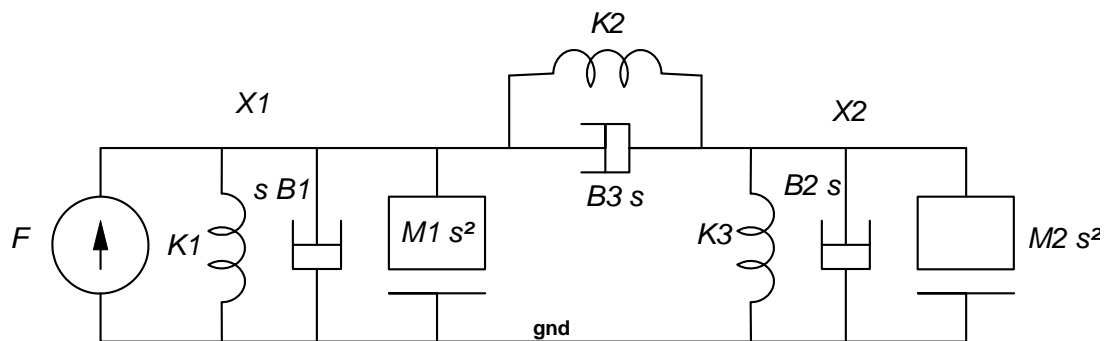
- Current is the analog of force, and
- Voltage is the analog of position, then
- The admittance is the analog of
 - Ms^2 (for a mass)
 - Bs (for friction)
 - K (for a spring)

This mass-spring system has three displacements. The circuit equivalent has three node voltages (X_1 , X_2 , X_3).

Each node has mass relative to ground (i.e. Einstein's theory of relativity)

The other nodes are the springs and friction

Redrawing this mass-spring circuit:



Writing the node equations then results in

$$(K_1 + B_1s + M_1s^2 + K_2 + B_3s)X_1 - (K_2 + B_3s)X_2 = F$$

$$(M_2s^2 + B_2s + K_3 + K_2 + B_3s)X_2 - (K_2 + B_3s)X_1 = 0$$

Solving for the highest derivative:

$$M_1s^2X_1 = -(K_1 + K_2 + B_1s + B_3s)X_1 + (K_2 + B_3s)X_2 + F$$

$$M_2s^2X_2 = -(B_2s + K_3 + K_2 + B_3s)X_2 + (K_2 + B_3s)X_1$$

The states (that which determines the energy in the system) are

- position, and
- velocity.

Defining the states this way results in the matrix formulation of dynamics (i.e. the state-space model) being:

$$s \begin{bmatrix} X_1 \\ X_2 \\ \cdots \\ sX_1 \\ sX_2 \end{bmatrix} = \begin{bmatrix} 0 & 0 & \vdots & 1 & 0 \\ 0 & 0 & \vdots & 0 & 1 \\ \cdots & \cdots & \cdots & \cdots & \cdots \\ \left(\frac{-(K_1+K_2)}{M_1}\right) & \left(\frac{K_2}{M_1}\right) & \vdots & \left(\frac{-(B_1+B_3)}{M_1}\right) & \left(\frac{B_3}{M_1}\right) \\ \left(\frac{K_2}{M_2}\right) & \left(\frac{-(K_2+K_3)}{M_2}\right) & \vdots & \left(\frac{B_3}{M_2}\right) & \left(\frac{-(B_2+B_3)}{M_2}\right) \end{bmatrix} \begin{bmatrix} X_1 \\ X_2 \\ \cdots \\ sX_1 \\ sX_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ \cdots \\ \left(\frac{1}{M_1}\right) \\ 0 \end{bmatrix} F$$

$$Y = X_2 = \begin{bmatrix} 0 & 1 & 0 & 0 \end{bmatrix} \begin{bmatrix} X_1 \\ X_2 \\ sX_1 \\ sX_2 \end{bmatrix} + [0]F$$

Note that

- You have 2N states, where N is the number of masses. Each mass has two energy states (kinetic and potential energy) giving your 2N state variables.
- The first N rows are [0 : I] where I is the identity matrix. This tells MATLAB that the states are position and velocity.
- The last N rows are where the dynamics come into play.

Also also, you can have real or complex poles for mass-spring systems - unlike the heat equation which always has real poles.

Finding the Transfer Function:

To find the transfer function, use MATLAB or SciLab. Assume for example that

- M = 1kg
- B = 2 Ns/m
- K = 10 N/m

Then the state-space model is:

$$s \begin{bmatrix} X_1 \\ X_2 \\ sX_1 \\ sX_2 \end{bmatrix} = \begin{bmatrix} 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \\ -20 & 10 & -4 & 2 \\ 10 & -20 & 2 & -4 \end{bmatrix} \begin{bmatrix} X_1 \\ X_2 \\ sX_1 \\ sX_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 1 \\ 0 \end{bmatrix} F$$

MATLAB Code: Input the A B C D matrices:

```
-->a11 = zeros(2,2);
-->a12 = eye(2,2);
-->a21 = [-20,10;10,-20];
-->a22 = [-4,2;2,-4];
-->A = [a11,a12;a21,a22]
```

```

0.    0.    1.    0.
0.    0.    0.    1.
- 20.   10.  - 4.    2.
10.   - 20.  2.   - 4.

```

```

-->B = [0;0;1;0];
-->C = [0,1,0,0];
-->D = 0;

```

Use these to define G(s):

```

-->G = ss(A,B,C,D)

```

Once G(s) is in MATLAB, find the transfer function

```

-->[z,p,k] = zpks(G)
k =
2.

p =
- 3. + 4.5825757i
- 3. - 4.5825757i
- 1. + 3.i
- 1. - 3.i

z =
- 5.

```

meaning:

$$X_2 = \left(\frac{2(s+5)}{(s+3 \pm j4.58)(s+1 \pm j3)} \right) F$$

If you want to approximate this with a 2nd-order model, keep the slowest pole and match the DC gain

```

-->DC = evalfr(G,0)
0.0333333

```

So

$$X_2 \approx \left(\frac{0.3333}{(s+1 \pm j3)} \right) F$$

To check the response in MATLAB, take the two step responses.

Input the 2nd-order approximation:

```

-->G2 = zpks([], [-1+j*3, -1-j*3], 0.3333)

```

Take the step response of the two systems:

```

-->t = [0:0.1:100]';
-->x2 = step(G,t);
-->x2a = step(G2,t);

```

and plot

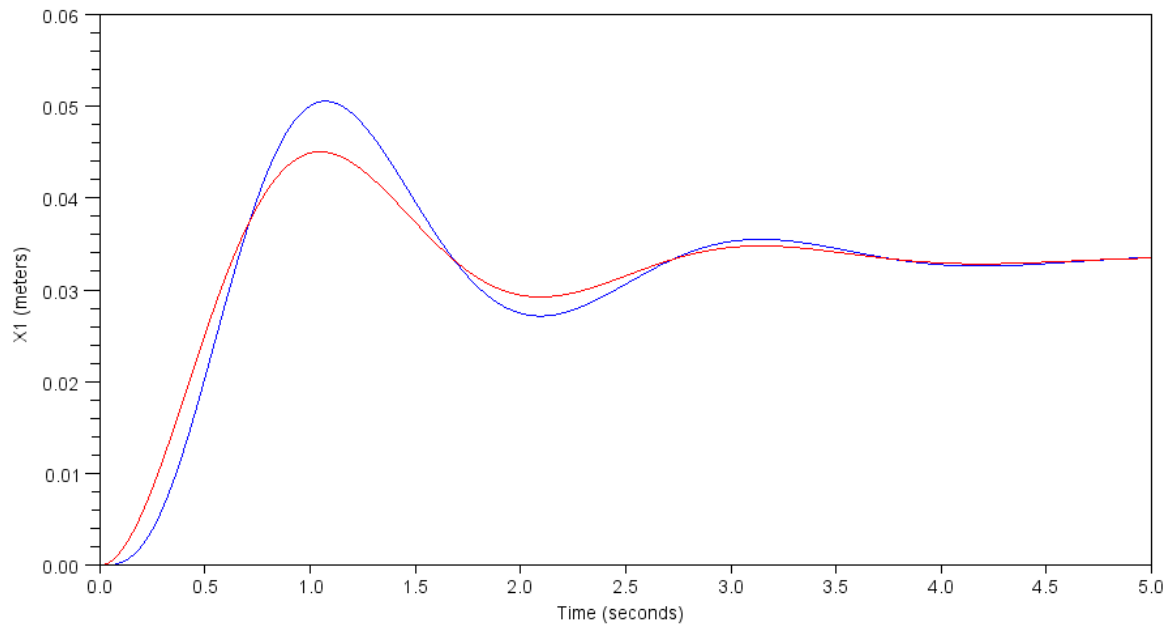
```

-->plot(t,x2,t,x2a)

```

```
-->xlabel('Time (seconds)');  
-->ylabel('X2 (meters)');
```

Note that the 2nd-order model isn't that good of an approximation: the 'fast' pole is only 3x faster.



Step Response of the 4th-Order Mass-Spring System (blue) and its 2nd-Order Approximation (red)

Matlab Code:

```

a11 = zeros(2,2);
a12 = eye(2,2);
a21 = [-20,10;10,-20];
a22 = [-4,2;2,-4];
A = [a11,a12;a21,a22]

```

```

    0    0    1    0
    0    0    0    1
   -20   10   -4    2
    10   -20    2   -4

```

```

B = [0;0;1;0];
C = [0,1,0,0];
D = 0;
G = ss(A,B,C,D);

```

```
zpk(G)
```

```

          2 (s+5)
-----
(s^2 + 2s + 10) (s^2 + 6s + 30)

```

```
tf(G)
```

```

          2 s + 10
-----
s^4 + 8 s^3 + 52 s^2 + 120 s + 300

```

$$X_2 = \left(\frac{2(s+5)}{(s+3 \pm j4.58)(s+1 \pm j3)} \right) F$$