
Servo-Compensators

Generalized Case

NDSU ECE 463/663

Lecture #18

Inst: Jake Glower

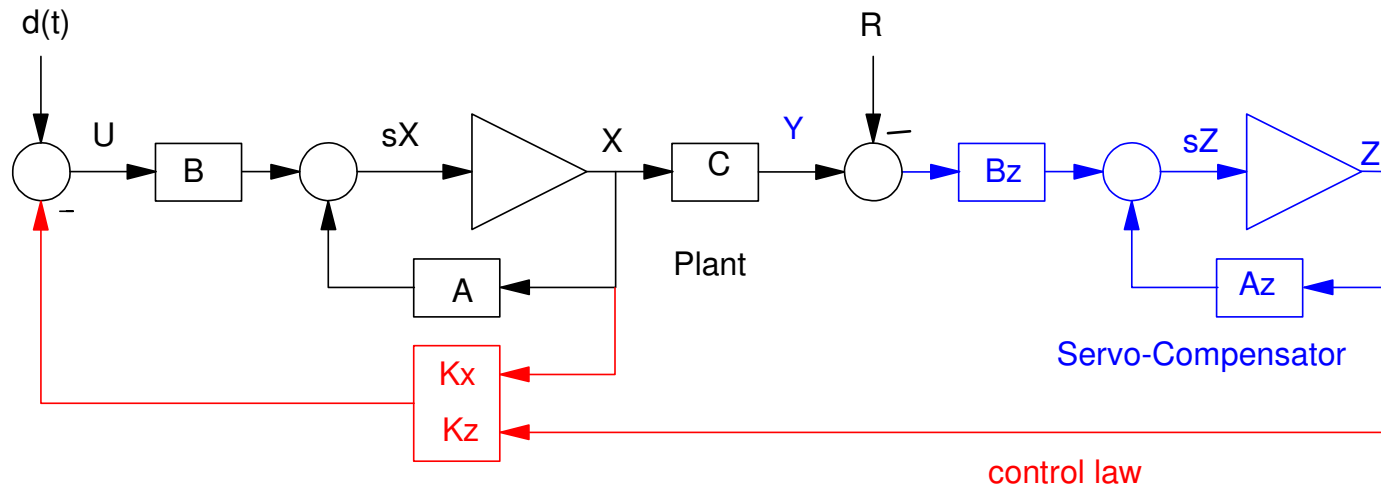
Please visit [Bison Academy](#) for corresponding
lecture notes, homework sets, and solutions

Recap

- If tracking or rejecting a constant, add a servo compensator with a pole at $s = 0$
- If tracking or rejecting a sinusoid, add a servo compensator with poles at $\pm j\omega$

Not surprisingly,

- If tracking or rejecting signals with poles at $\{ 0, j\omega, -j\omega \}$, add a servo compensator with poles at $\{ 0, j\omega, -j\omega \}$.



State-Space Formulation: Let the plant be

$$sX = AX + BU + Bd$$

$$Y = CX$$

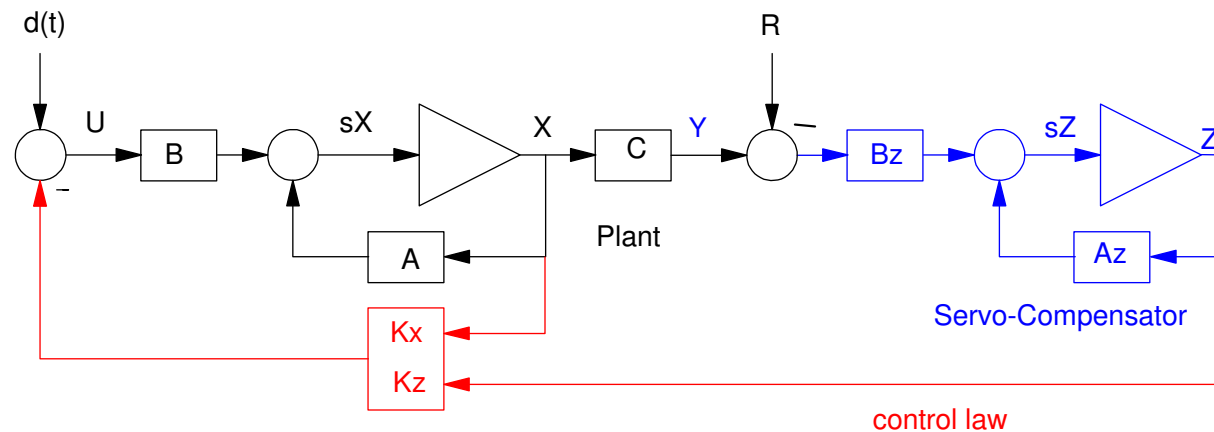
Define a servo-compensator

$$sZ = A_z Z + B_z(Y - R)$$

so that the eigenvalue of A_z are

$$eig(A_z) = 0, \pm j\omega$$

Feed the servo-compensator with the difference between Y and the set point R



In state-space, the plant plus servo-compensator looks like the following:

$$s \begin{bmatrix} X \\ Z \end{bmatrix} = \begin{bmatrix} A & 0 \\ B_z C & A_z \end{bmatrix} \begin{bmatrix} X \\ Z \end{bmatrix} + \begin{bmatrix} B \\ 0 \end{bmatrix} U + \begin{bmatrix} 0 \\ -B_z \end{bmatrix} R + \begin{bmatrix} B \\ 0 \end{bmatrix} d$$

$$U = - \begin{bmatrix} K_x & K_z \end{bmatrix} \begin{bmatrix} X \\ Z \end{bmatrix}$$

or you can write this as

$$s \begin{bmatrix} X \\ Z \end{bmatrix} = \begin{bmatrix} A - BK_x & -BK_z \\ B_z C & A_z \end{bmatrix} \begin{bmatrix} X \\ Z \end{bmatrix} + \begin{bmatrix} 0 \\ -B_z \end{bmatrix} R + \begin{bmatrix} B \\ 0 \end{bmatrix} d$$

Example:

Assume a 4th-order heat equation:

$$sX = \begin{bmatrix} -2 & 1 & 0 & 0 \\ 1 & -2 & 1 & 0 \\ 0 & 1 & -2 & 1 \\ 0 & 0 & 1 & -1 \end{bmatrix} X + \begin{bmatrix} 1 \\ 0 \\ 0 \\ 0 \end{bmatrix} U + \begin{bmatrix} 1 \\ 0 \\ 0 \\ 0 \end{bmatrix} d(t)$$
$$Y = \begin{bmatrix} 0 & 0 & 0 & 1 \end{bmatrix} X$$

Design a feedback control law for the following system so that

- The 2% settling time is 13 seconds,
 - There is no overshoot for a step input,
 - Y tracks a constant setpoint (R = 1), and
 - Y rejects a sinusoidal disturbance at 1 rad/sec
-

Note: The result works for any combination of DC and 1 rad/sec:

$$R(t) = a_1 + b_1 \cos(t) + c_1 \sin(t)$$

$$d(t) = a_2 + b_2 \cos(t) + c_2 \sin(t)$$

Step 1: Add a servo compensator:

- Controllable
- Poles at $\{0, j, -j\}$

$$sZ = \begin{bmatrix} 0 & 1 & \vdots & 0 \\ -1 & 0 & \vdots & 0 \\ \cdots & \cdots & \vdots & \cdots \\ 0 & 0 & \vdots & 0 \end{bmatrix} Z + \begin{bmatrix} 1 \\ 1 \\ \cdots \\ 1 \end{bmatrix} (R - Y)$$

Step 2: Create the augmented system: plant + servo compensator

$$s \begin{bmatrix} X \\ Z \end{bmatrix} = \begin{bmatrix} A & 0 \\ B_z C & A_z \end{bmatrix} \begin{bmatrix} X \\ Z \end{bmatrix} + \begin{bmatrix} B \\ 0 \end{bmatrix} U + \begin{bmatrix} 0 \\ -B_z \end{bmatrix} R + \begin{bmatrix} B \\ 0 \end{bmatrix} d$$

$$s \begin{bmatrix} X \\ \dots \\ Z \end{bmatrix} = \begin{bmatrix} -2 & 1 & 0 & 0 & \vdots & 0 & 0 & 0 \\ 1 & -2 & 1 & 0 & \vdots & 0 & 0 & 0 \\ 0 & 1 & -2 & 1 & \vdots & 0 & 0 & 0 \\ 0 & 0 & 1 & -1 & \vdots & 0 & 0 & 0 \\ \dots & \dots & \dots & \dots & \vdots & \dots & \dots & \dots \\ 0 & 0 & 0 & 1 & \vdots & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 & \vdots & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 & \vdots & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} X \\ \dots \\ Z \end{bmatrix} + \begin{bmatrix} 1 \\ 0 \\ 0 \\ 0 \\ \dots \\ 0 \\ 0 \\ 0 \end{bmatrix} U + \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ \dots \\ -1 \\ -1 \\ -1 \end{bmatrix} R + \begin{bmatrix} 1 \\ 0 \\ 0 \\ 0 \\ \dots \\ 0 \\ 0 \\ 0 \end{bmatrix} d$$

Design a full-state feedback control law to meet the design specs.

- Dominant pole at $s = -1$
- Place the poles at $\{-1, -2, -2.2, -2.3, -2.4, -0.3+j, -0.3-j\}$ using Bass Gura

In Matlab:

$$A = [-2, 1, 0, 0; 1, -2, 1, 0; 0, 1, -2, 1; 0, 0, 1, -1]$$

$$\begin{array}{cccc} -2 & 1 & 0 & 0 \\ 1 & -2 & 1 & 0 \\ 0 & 1 & -2 & 1 \\ 0 & 0 & 1 & -1 \end{array}$$

$$B = [1; 0; 0; 0]$$

$$\begin{array}{c} 1 \\ 0 \\ 0 \\ 0 \end{array}$$

$$C = [0, 0, 0, 1]$$

$$\begin{array}{cccc} 0 & 0 & 0 & 1 \end{array}$$

$$Az = [0, 1, 0; -1, 0, 0; 0, 0, 0]$$

$$\begin{array}{ccc} 0 & 1 & 0 \\ -1 & 0 & 0 \\ 0 & 0 & 0 \end{array}$$

$$Bz = [1; 1; 1]$$

$$\begin{array}{c} 1 \\ 1 \\ 1 \end{array}$$

$$A7 = [A, \text{zeros}(4, 3) ; Bz * C, Az]$$

$$\begin{array}{ccccccc} -2 & 1 & 0 & 0 & : & 0 & 0 & 0 \\ 1 & -2 & 1 & 0 & : & 0 & 0 & 0 \\ 0 & 1 & -2 & 1 & : & 0 & 0 & 0 \\ 0 & 0 & 1 & -1 & : & 0 & 0 & 0 \\ \hline 0 & 0 & 0 & 1 & : & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 & : & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 & : & 0 & 0 & 0 \end{array}$$

```
B7u = [B ; zeros(3,1)]
```

```
    1  
    0  
    0  
    0  
- - - - -  
    0  
    0  
    0
```

```
K7 = ppl(A7, B7u, [-1, -2, -2.2, -2.3, -2.4, -0.3+j, -0.3-j])
```

```
    3.5000    12.0900    29.6810    63.4358    0.5236    21.3719    26.4739
```

This gives

```
Kx = [ 3.5000    12.0900    29.6810    63.4358 ]
```

```
Kz = [ 0.5236    21.3719    26.4739 ]
```

Step Responses

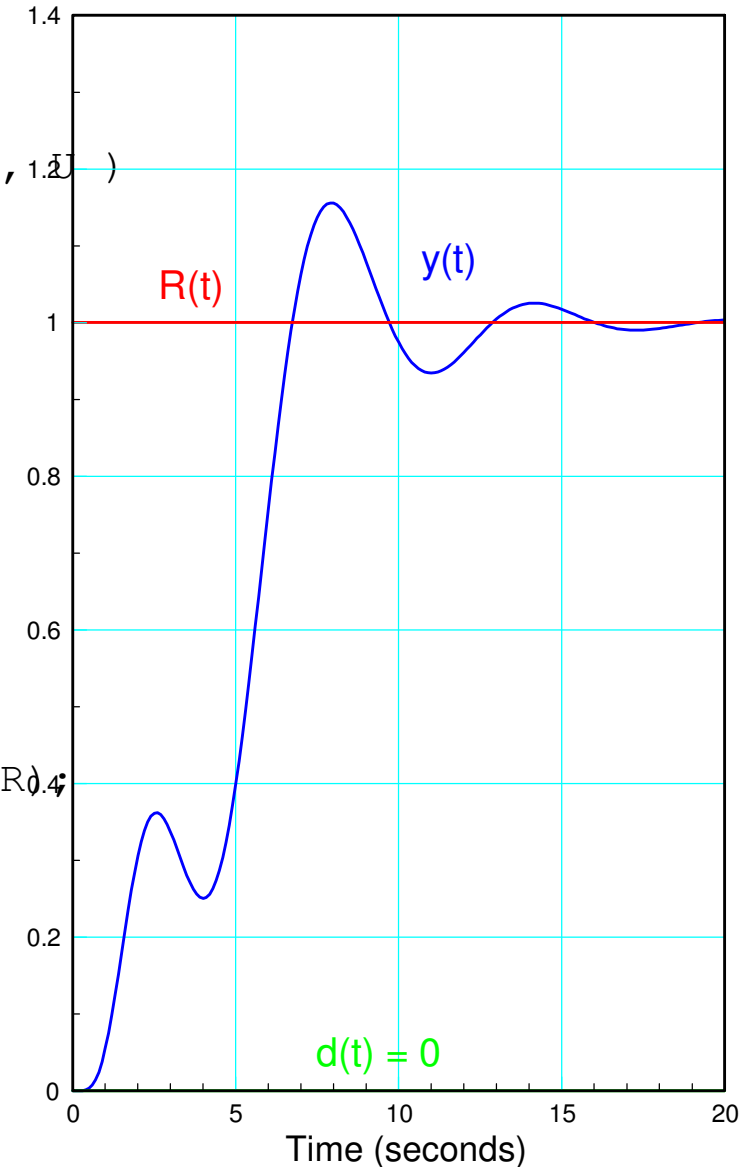
- Use the *step2* command from before

```
function [ y ] = step3( A, B, C, D, t, X0, R )
```

Case 1: Step Response with Respect to R

- The system tracks a constant set point:

```
B7r = [0*B ; -Bz];  
C7 = [C, zeros(1,3)];  
D7 = 0;  
X0 = zeros(7,1);  
t = [0:0.1:20]';  
R = 0*t + 1;  
y = step3(A7-B7u*K7, B7r, C7, D7, t, X0, R);  
plot(t,R,'r',t,y,'b')
```



Case 2: Response to disturbance, d

- Rejects a 1 rad/sec disturbance

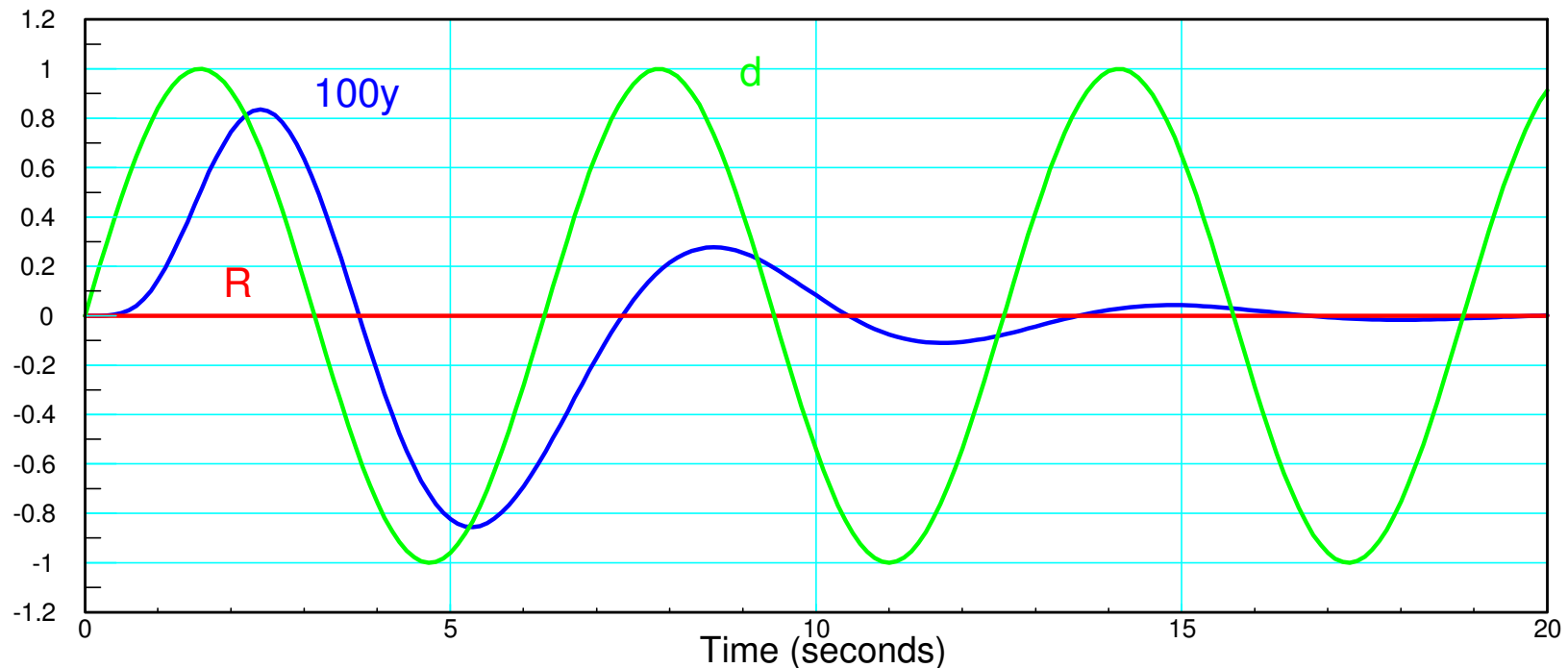
```
B7d = [B ; 0*Bz];
```

```
R = 0*t;
```

```
d = sin(t);
```

```
y = step3(A7-B7u*K7, B7d, C7, D7, t, X0, d);
```

```
plot(t,R,'r',t,y,'b',t,d,'g')
```



Case 3: Constant Set Point & 1 rad/sec Noise

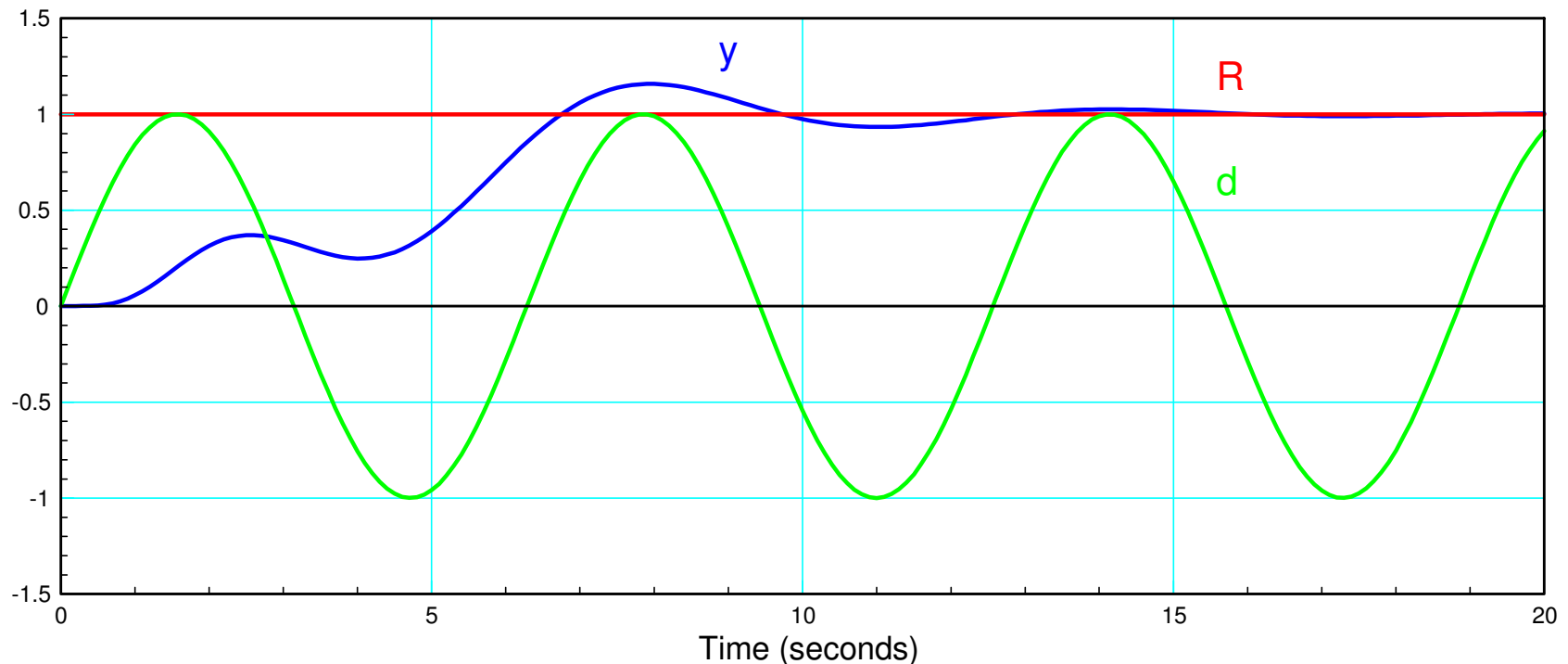
- Tracks a constant set point, rejects a 1 rad/sec disturbance

```
d = sin(t);
```

```
R = 0*t + 1;
```

```
y = step3(A7-B7u*K7, [B7r, B7d], C7, [0,0], t, X0, [R,d]);
```

```
plot(t,R,'r',t,y,'b',t,d,'g')
```

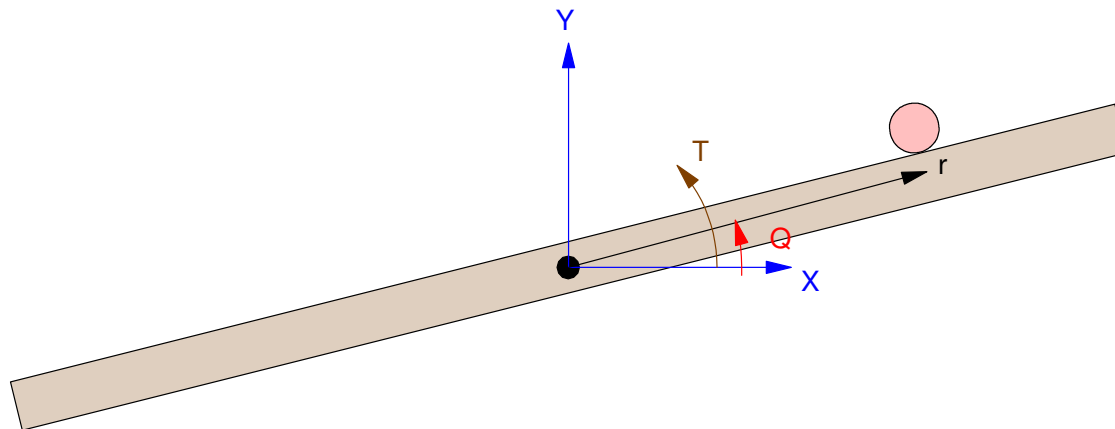


Example 2: Ball and Beam System

- $m = 1.1\text{kg}$ (0.1kg more than than the model)
- $R(t) = 1.0 - 0.4 \cos(t)$

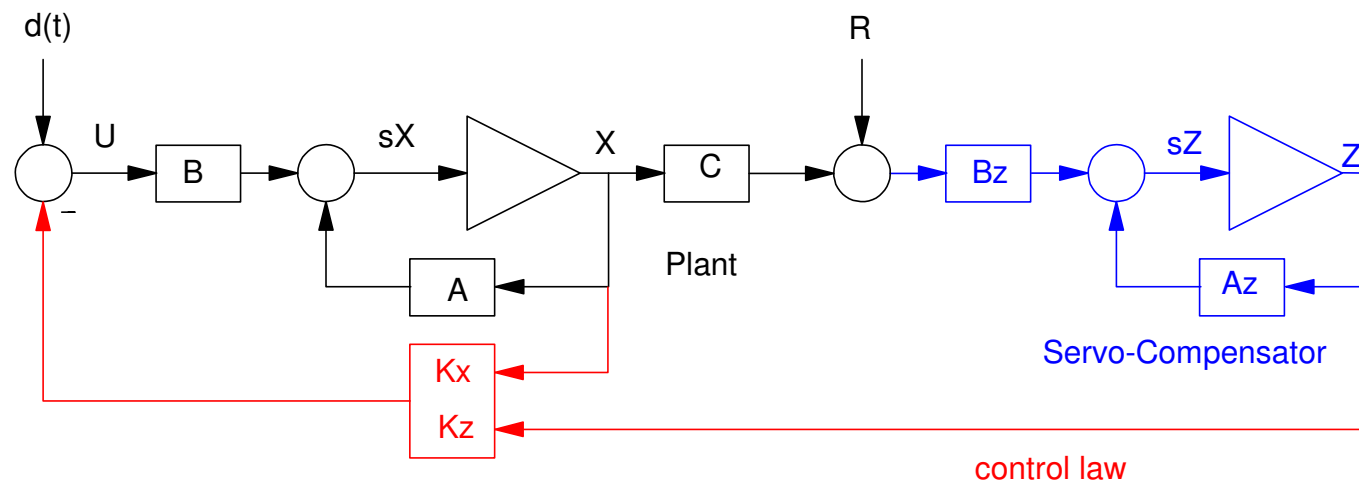
Extra mass creates

- A constant disturbance due to gravity, plus
- A 1 rad/sec disturbance



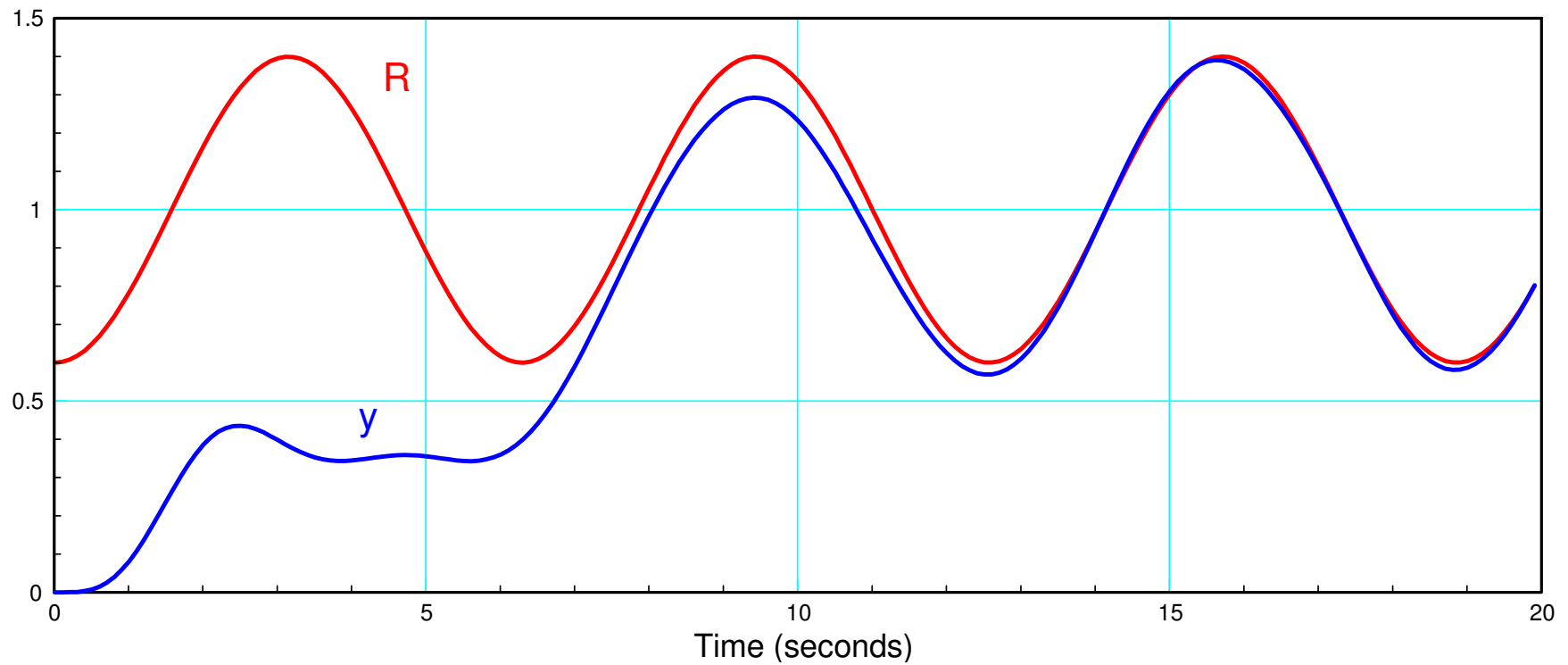
Same solution as before

- Add a servo compensator
- Pick A_z to have poles at $\{0, -j, +j\}$
- Pick K_x and K_z to place the closed-loop poles



Result: $m = 1.1\text{kg}$

- Tracks a constant & 1 rad/sec sine wave
- Rejects disturbances at DC and 1 rad/sec

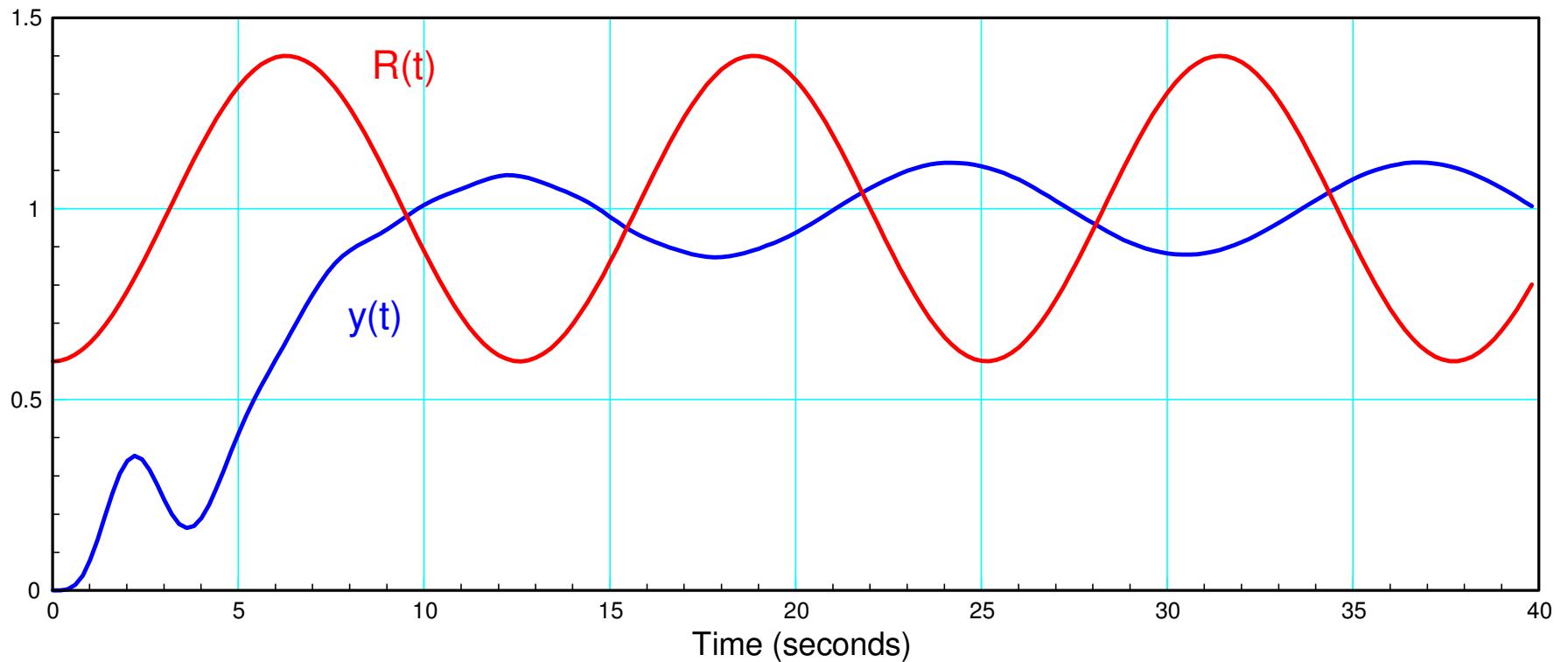


Sidelight: What is the frequency changes?

- Change the frequency to 0.5 rad/sec

No longer tracks

- Not designed for 0.5 rad/sec



What to do?

Option 1:

- Determine the frequency of $R(t)$
- Redesign the servo compensator

Option 2:

- Pick A_z to have poles at $\{0, j0.5, j, j1.5, j2\}$
- Results in a 9th-order compensator

Option 3: Adaptive Control

- Estimate the frequency of $R(t)$ in real time
- Change A_z , K_x , K_z accordingly

Option 4: Adaptive Control (Self-Tuning Regulator)

- Estimate the next value of $R(t)$ in real time
- Determine the input to drive $y(t)$ to $R(t)$ in real time

There are more options...

Summary

If you are trying to track a constant and/or reject a constant disturbance

- Add a servo compensator with a pole at $s = 0$.

If you are trying to track and/or reject a sinusoidal

- Add a servo compensator with poles at $\{+j\omega, -j\omega\}$

If you are trying to do both

- Add a servo compensator with poles at $\{0, +j\omega, -j\omega\}$

This can result in a very high order compensator

- The step response can be pretty squirrely as the compensator tries to figure out what you're trying to track
-