# Pole Placement (Bass Gura)

#### NDSU ECE 463/663

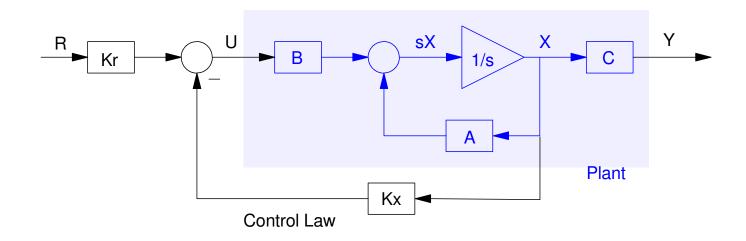
# Lecture #13 Inst: Jake Glower

Please visit Bison Academy for corresponding lecture notes, homework sets, and solutions

## **Pole Placement**

If a system is controllable, Kx can place all N poles of the closed-loop system anywhere.

- How do you find Kx?
- How do you find Kr?



## **Definitions:**

Open-Loop System: System dynamics with U = 0. sX = AX

Closed-Loop System: System dynamics with U = -Kx X $sX = (A - BK_x)X$ 

Characteristic Polynomial:

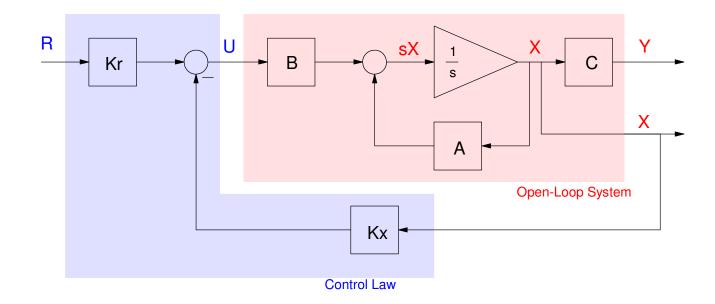
- a) The polynomial with roots equal to the eigenvalues of A poly(eig(A))
- b) The denominator polynomial of the transfer function

## **Bass Gura Derivation:**

Assume

- A system is controllable.
- Full-state feedback is used:

 $U = K_r R - K_x X$ 



Problem: Find Kx and Kr to Place the Poles of the Closed-Loop System and Set the DC Gain from R to Y

## **Case 1: Controller Canonical Form:**

Assume the system is in controller canonical form

• Characteristic polynomial (i.e. the denominator of the transfer function) is  $P(s) = s^4 + a_3 s^3 + a_2 s^2 + a_1 s + a_0$ 

Find the feedback gains so that the characteristic polynomial becomes

$$P_d(s) = s^4 + b_3 s^3 + b_2 s^2 + b_1 s + b_0$$

In controller canonical form, the plant is:

$$sX = \begin{bmatrix} 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \\ -a_0 & -a_1 & -a_2 & -a_3 \end{bmatrix} X + \begin{bmatrix} 0 \\ 0 \\ 0 \\ 1 \end{bmatrix} U$$

With full-state feedback:

$$U = - \begin{bmatrix} k_0 & k_1 & k_2 & k_3 \end{bmatrix} X$$

the dynamics become

$$sX = \begin{bmatrix} 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \\ -a_0 - k_0 & -a_1 - k_1 & -a_2 - k_2 & -a_3 - k_3 \end{bmatrix} X$$

By inspection, the closed-loop characteristic polynomial is:  $s^4 + (a_3 + k_3)s^3 + (a_2 + k_2)s^2 + (a_1 + k_1)s + (a_0 + k_0) = 0$ 

which is to be equal to the desired characteristic polynomial:

$$s^4 + b_3 s^3 + b_2 s^2 + b_1 s + b_0 = 0$$

Match terms

• The feedback gains are the difference between the desired and open-loop characteristic polynomials.

$$k_{3} = b_{3} - a_{3}$$
  

$$k_{2} = b_{2} - a_{2}$$
  

$$k_{1} = b_{1} - a_{1}$$
  

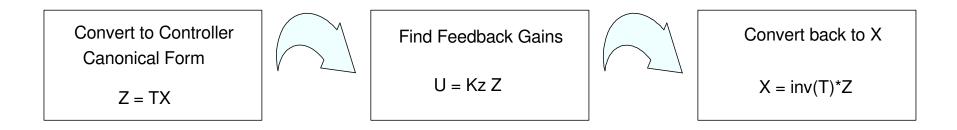
$$k_{0} = b_{0} - a_{0}$$

#### Case 2: The system not in controller canonical form

If this is the case,

- Find a similarity transform, T, which takes you to controller canonical form
- Find the feedback gains to place the closed-loop poles in controller form
- Convert these feedback gains to state-variable form with this similarity transform.

This method is called Bass-Gura or Pole Placement.



### Bass Gura: Step 1

Find a similarity transform which takes you to controller canonical form.

 $T = T_1 T_2 T_3$ 

T1 is the controllability matrix (assume a 4th-order system here):

 $T_1 = \left[ B A B A^2 B A^3 B \right]$ 

T2 is related to the system's characteristic polynomial

$$det (sI - A) = s^{4} + a_{3}s^{3} + a^{2}s^{2} + a_{1}s + a_{0}$$
$$T_{2} = \begin{bmatrix} 1 & a_{3} & a_{2} & a_{1} \\ 0 & 1 & a_{3} & a_{2} \\ 0 & 0 & 1 & a_{3} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

T3 is a flip matrix  
$$T_{3} = \begin{bmatrix} 0 & 0 & 0 & 1 \\ 0 & 0 & 1 & 0 \\ 0 & 1 & 0 & 0 \\ 1 & 0 & 0 & 0 \end{bmatrix}$$

This similarity transform results in the transformed system being

$$Z = TX$$
  
$$sZ = (T^{-1}AT)Z + (T^{-1}B)U$$

or

$$sZ = A_zZ + B_zU$$

where (Az, Bz) are in controller canonical form.

Note that since T includes the controllability matrix and T is inverted, the (A, B) must be controllable for this algorithm to work.

#### Bass Gura: Step 2

Determine the feedback gains in controller form (Kz)

• This is the difference between the desired and actual characeristic polynominals

**Open-Loop Characteristic Polynomial:** 

 $P(s) = s^4 + a_3s^3 + a_2s^2 + a_1s + a_0$ 

Closed-Loop (desired) Characteristic Polynomial:  $P_d(s) = s^4 + b_3 s^3 + b_2 s^2 + b_1 s + b_0$ 

Feedback Gains:

$$K_z = \left[ (b_0 - a_0), (b_1 - a_1), (b_2 - a_2), (b_3 - a_3) \right]$$

### **Bass Gura: Step 3**

Convert back to state-variable form (X) using the similarity transform:

 $K_x = K_z T^{-1}$ 

Check your answer. The closed-loop system is then

 $sX = (A - BK_x)X$ 

The eigenvalues of (A - BK) should be where you wanted to place them.

### Step 4: Set the DC Gain (Find Kr)

Assume

 $U = K_r R - K_x X$ 

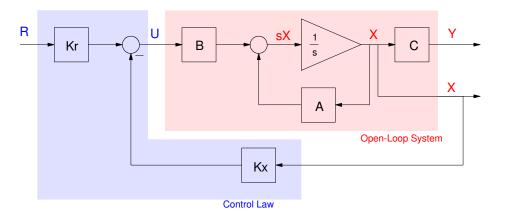
then the closed-loop dynamics are

 $sX = (A - BK_x)X + BK_rR$ Y = CX

The steady-state (i.e. DC) gain is  $sX = 0 = (A - BK_x)X + BK_rR$   $X = -(A - BK_x)^{-1}BK_rR$  $Y = -C(A - BK_x)^{-1}BK_rR$ 

Pick Kr so that

 $-C(A - BK_x)^{-1}BK_r = 1$ 



## **Example 1: Heat Equation.**

Assume a system has the following dynamics:

$$sX = \begin{bmatrix} -2 & 1 & 0 & 0 \\ 1 & -2 & 1 & 0 \\ 0 & 1 & -2 & 1 \\ 0 & 0 & 1 & -1 \end{bmatrix} X + \begin{bmatrix} 1 \\ 0 \\ 0 \\ 0 \end{bmatrix} U$$

Find the feedback gain, Kx, to place the poles of the closed-loop system

$$U = -K_X X$$

at { -1, -2, -3, -4 }

📣 MATLAB 7.12.0 (R2011a) File Edit Debug Desktop Window Help 🎦 🗂 👗 🐂 📋 🤊 🥲 🐞 🛒 📄 🔞 C:\Documents and Settings\Admi Shortcuts 🛃 How to Add 🛛 🛃 What's New >> A = [-2, 1, 0, 0; 1, -2, 1, 0; 0,A = -2 1 0 0 1 -2 1 0 0 1 -2 1 1 -1 Ο 0 >> B = [1;0;0;0]В = 1 0 0 0 *fx* >>

Step 1: Find the similarity transform which takes you to controller canonical form.

T1 is the controllability matrix:

The system is controllable

T2 is related to the system's characteristic polynomial

>> P = poly(eig(A))1.0000 7.0000 15.0000 10.0000 1.0000 >> T2 = [P(1:4); 0, P(1:3); 0, 0, P(1:2); 0, 0, 0, P(1)]1.0000 7.0000 15.0000 10.0000 1.0000 7.0000 15.0000 0 1.0000 7.0000 0 0 0 0 1.0000 0

#### T3 is a flip matrix

>> T3 = [0,0,0,1;0,0,1,0;0,1,0,0;1,0,0,0]

0	0	0	1
0	0	1	0
0	1	0	0
1	0	0	0

The transform to controller canonical form is:

```
>> T = T1*T2*T3;
>> Az = inv(T) *A*T
          1.0000
        0
                           0
                                    0
                   1.0000
          -0.0000
        0
                            0.0000
            0.0000 0.0000 1.0000
        0
  -1.0000 -10.0000 -15.0000
                            -7.0000
>> Bz = inv(T)*B;
        0
        0
        0
        1
```

Check: (Az, Bz) are in controller canonical form.

Step 2: Find the full-state feedback gains in controller form.

• The difference between the desired and open-loop characteristic polynomials:

>> Pd = poly([-1, -2, -3, -4])					
1	10	35	50	24	
>> P = poly(eig(A))					
1	7	15	10	1	
>> dP = Pd - P					
0	3	20	40	23	
>> Kz = dP([5,4,3,2])					
23	40	20	3		

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	>> T1 = [B, A*B, A*A*B, A*A*A*B
	>> P = poly(eig(A));
	>> T2 = $[P(1:4); 0, P(1:3);$
	>> T3 = $[0, 0, 0, 1; 0, 0, 1, 0; 0, 1, 0]$
	>> T = T1*T2*T3;
	>> Pd = poly([-1, -2, -3, -4]);
	>> P = poly(eig(A));
	>> dP = Pd - P;
	>> $Kz = dP([5, 4, 3, 2]);$
	>> Az = inv(T)*A*T;
	>> Bz = inv(T)*B;
	>> eig(Az – Bz*Kz)
	ans =
	-4.0000
	-3.0000
	-2.0000
	-1.0000

Step 3: Convert Kz to the gain times the state variables (X)

```
>> Kx = Kz*inv(T)
3.0000 5.0000 7.0000 8.0000
>> eig(A - B*Kx)
-4.0000
-3.0000
-2.0000
-1.0000
```

The control law which places the closed-loop poles at  $\{-1, -2, -3, -4\}$  is

$$U = -K_x X$$

where

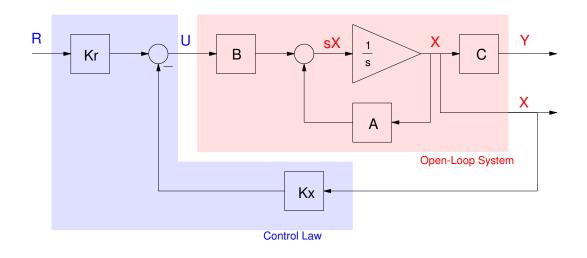
$$K_x = \left[ \begin{array}{ccc} 3 & 5 & 7 & 8 \end{array} \right]$$

#### Finding Kr:

$$-C(A - BK_x)^{-1}BK_r = 1$$
>> DC = -C\*inv(A-B\*Kx)\*B
DC = 0.0417
>> Kr = 1/DC
Kr = 24.0000

So the control law is

$$U = K_r R - K_x X$$
$$K_r = 24$$
$$K_x = \begin{bmatrix} 3 5 7 8 \end{bmatrix}$$

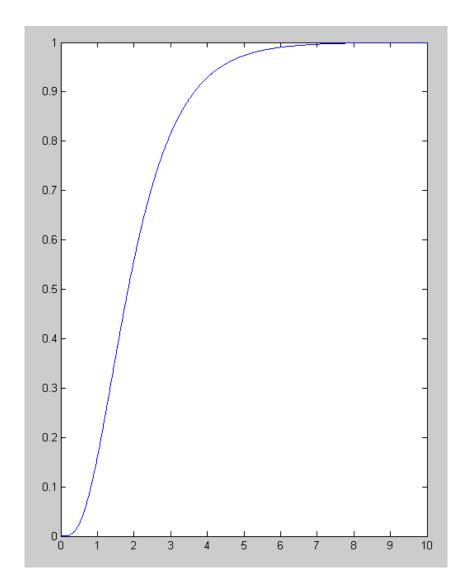


#### Plotting the Step Response

```
>> t = [0:0.01:10]';
>> G = ss(A-B*Kx, B*Kr, C, 0);
>> y = step(G,t);
>> plot(t,y);
```

Note:

- The DC gain is 1.000
- The 2% settling time is 4ish seconds
  Dominant pole is at -1
- No overshoot for step input
  - Dominant pole is real



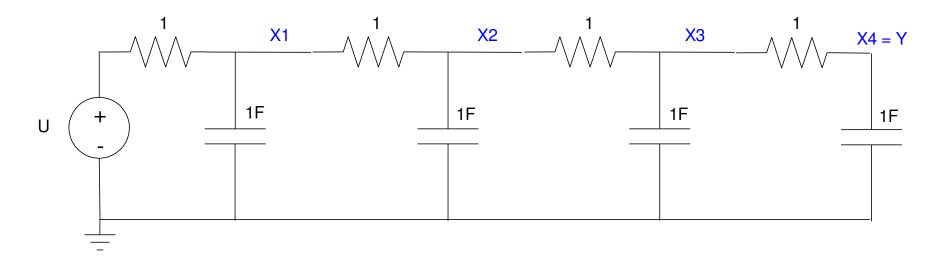
#### **Example 2: Complex Poles**

You can place the poles *anywhere* with pole placement

You can even make an RC circuit oscillate

Example: Place the closed-loop poles at

 $\{ -1 + j3, -1 - j3, -5 + j2, -5 - j2 \}$ 



#### **Bass Gura**

- Step 0: Input the system (done)
- Step 1: Find the similarity transform (done)
- Step 2: Find the feedback gains, Kz

>> Pd = poly([-1 + j\*3, -1 - j\*3, -5 + j\*2, -5-j\*2])
 1 12 59 158 290
>> P = poly(eig(A))
 1.0000 7.0000 15.0000 10.0000 1.0000
>> dP = Pd - P
 0 5 44 148 289
>> Kz = dP([5,4,3,2])
 289 148 44 5

#### Step 3: Convert Kz to Kx:

 $>> Kx = Kz \star inv(T)$ 

5.0000 19.0000 61.0000 204.0000

#### Check Kx:

>> eig(A - B\*Kx)

-5.0000 + 2.0000i -5.0000 - 2.0000i -1.0000 + 3.0000i -1.0000 - 3.0000i

#### Find Kr

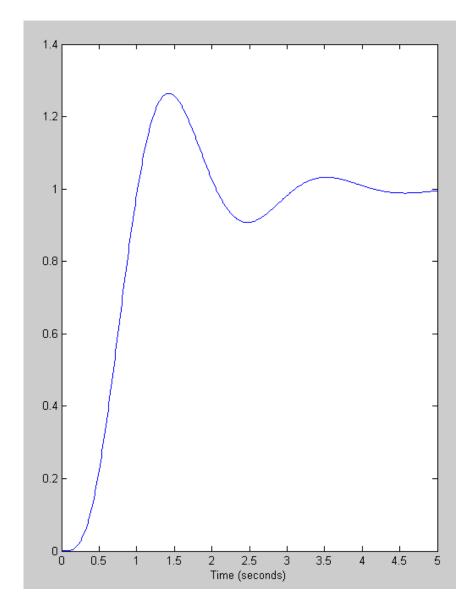
>> DC = -C\*inv(A-B\*Kx)\*B
DC = 0.0034
>> Kr = 1/DC
Kr = 290.0000

So the resulting control law is:

$$U = K_r R - K_x X$$
  

$$K_r = 290$$
  

$$K_x = \begin{bmatrix} 5 \ 19 \ 61 \ 204 \end{bmatrix}$$

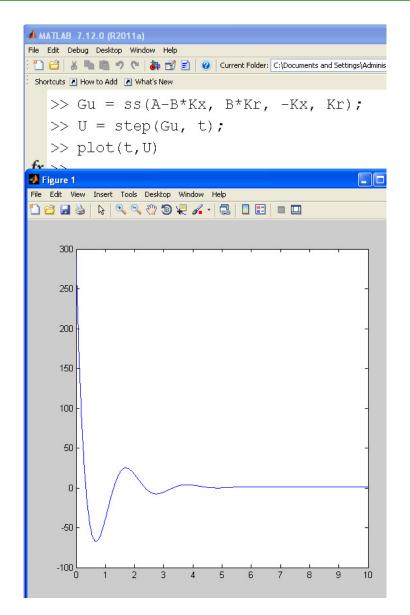


# How is this possible?

In Thrust we Trust

Raw power.

- Large feedback gains tell you you're trying to force the system to behave contrary to its nature
- In theory, it can be done
- In practice, it takes a lot of power



## How is this used?

https://asian-defence.blogspot.com/2011/05/russia-experts-says-russia-could-sell.html http://iptmajor.weebly.com/uploads/3/8/3/2/38326191/2319116\_orig.jpg

With full-state feedback, any response is possible

- You can make a MIG behave like an F-14
- You can make a research-grade robot behave like an assembly-line robot

Bass Gura allows you to find full-state feedback gains to place the closed-loop poles *anywhere*.



