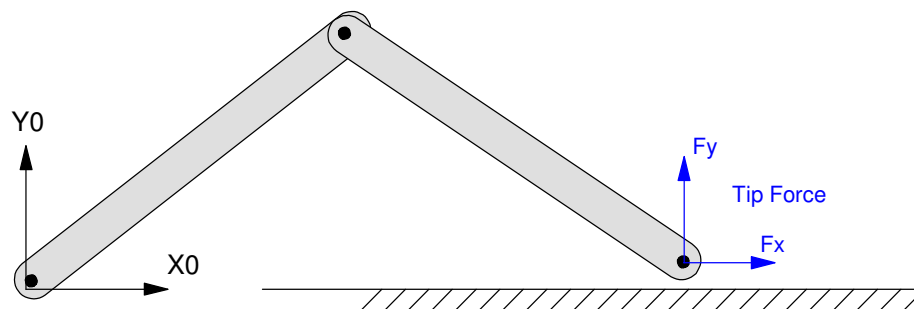


Impact Forces

Trying to control the motion of a robot in contact with the environment, such as a hard rigid floor at $y=0$, is easy if the robot is stationary. It is very hard if the robot is in motion, such as polishing the floor.

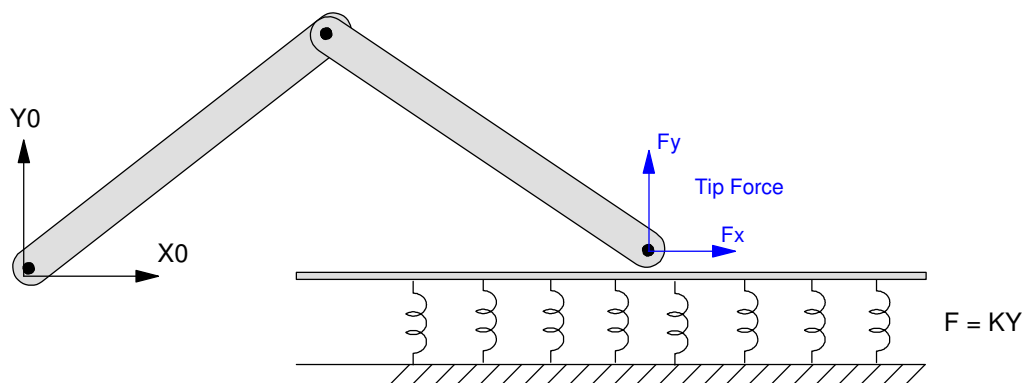


Tip Constraint: The robot motion is constrained by the floor at $y = 0$

One way around the problem of dealing with a hard constraint, such as

$$y_2 \geq 0$$

is to remove that constraint and replace it with a spring - essentially making the floor a spring



Now, the tip is allowed to go below zero - sinking into the floor slightly. When it does so, a tip force results, opposing the robot. This tip force then translates to the joint torques through the Jacobian as

$$T = J^T F_{tip}$$

With this approach, you can polish a floor with a desired force.

Example: Move back and forth from $x_2 = 0.5$ to $x_2 = 1.5$ with a force of 10N.

Solution: Specify the motion of the robot to be

$$x_{2ref} = \left(\frac{1 - \cos(\pi t)}{2} \right) + 0.5$$

$$y_{2ref} = 0$$

Using the previous Cartesian control, this results in the robot moving back and forth on the surface with no force.

Add a spring constant to the floor (100 N/m chosen as a fairly stiff floor. Friction is added for a lossy floor)

$$F_{floor} = \min(0, 100x_2 + 20\dot{x}_2)$$

In the X direction, control the robot using a PID control law so that the robot follows the desired path

$$F_x = 16(x_{2ref} - x_2) + 6(\dot{x}_{2ref} - \dot{x}_2)$$

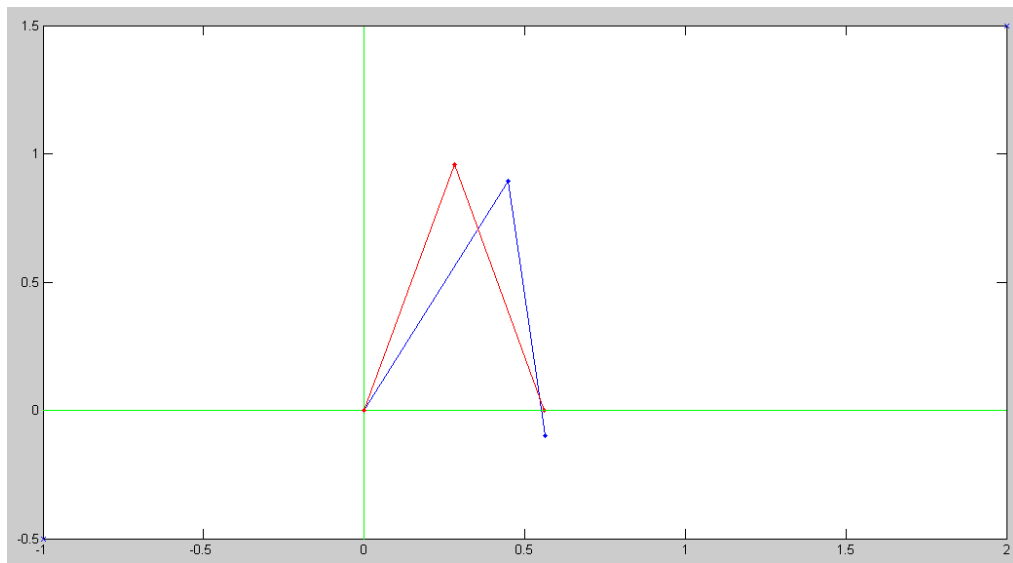
In the Y direction, add a bias to the force so that robot leans into the floor, providing 10N of force

$$F_y = 100 \int (10 - F_{floor}) dt$$

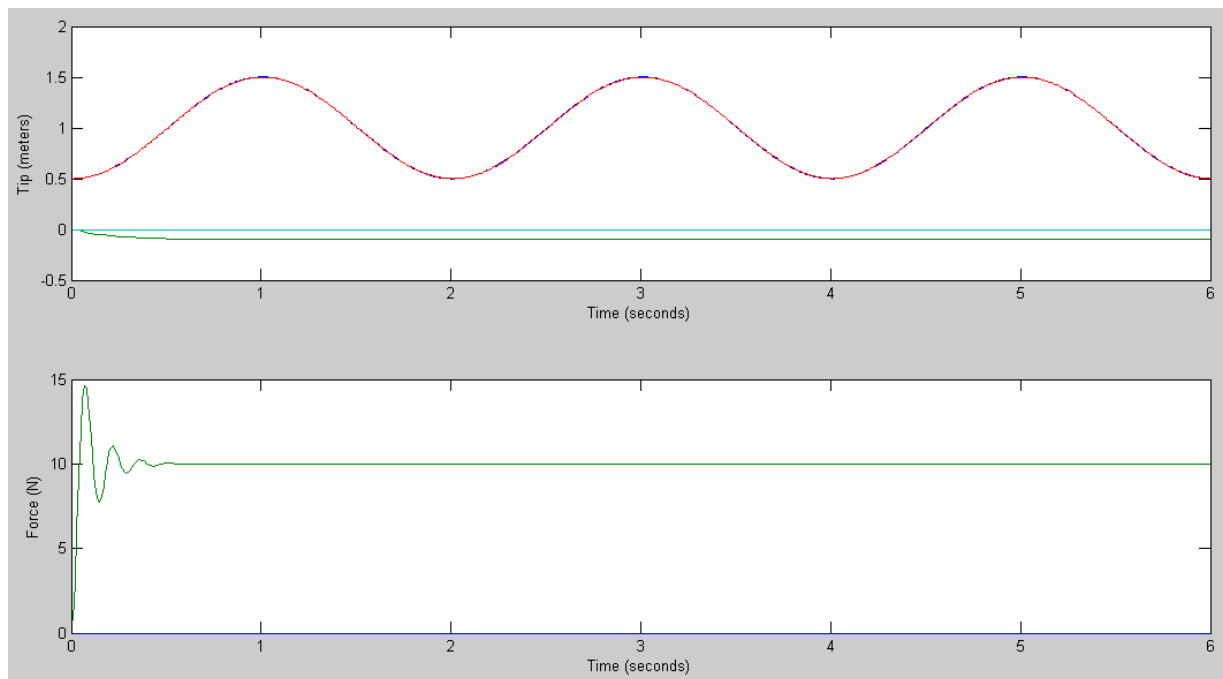
The joint torques are then computed using the Jacobian

$$T = J^T \begin{bmatrix} F_x \\ F_y \end{bmatrix}$$

Simulation Results (RR_XY_Floor_Control.txt)



Desired Motion of the Robot (red) and Actual (Blue). The robot sinks into the floor so that 10N of force is applied



Resulting tip position and tip force. The tip force is regulated at 10N as desired.

Impact Forces

Develop a control law that

- Starts out above the floor $P0 = (0.5, 0.5)$
- Moves to the floor $P1 = (0.5, 0)$
- Moves 1m to $P2 = (1.5, 0)$
- with a force of 10N
- Lifts up from the floor to $P3 = (1.5, 0.5)$
- Moves back to $P0$,

and repeat traces out a square with the corners at

Method #1: You don't really have to change anything at this point. Just specify the points on the floor as being below the surface and you'll get a force. The distance into the floor you need to go depends upon the net spring constant

$$K_{net} = K_{floor} || K_{pid}$$

where

K_{pid} is the P gain for your PID control law.

For example, let

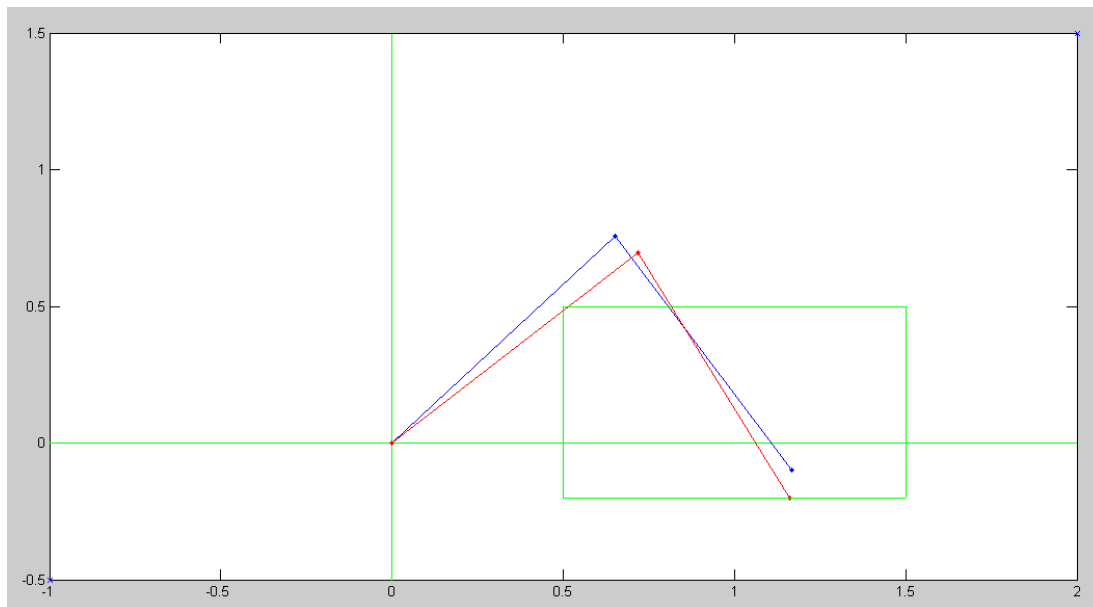
$$K_{floor} = 100$$

$$PID = 100(y_{2ref} - y_2) + 20(\dot{y}_{2ref} - \dot{y}_2)$$

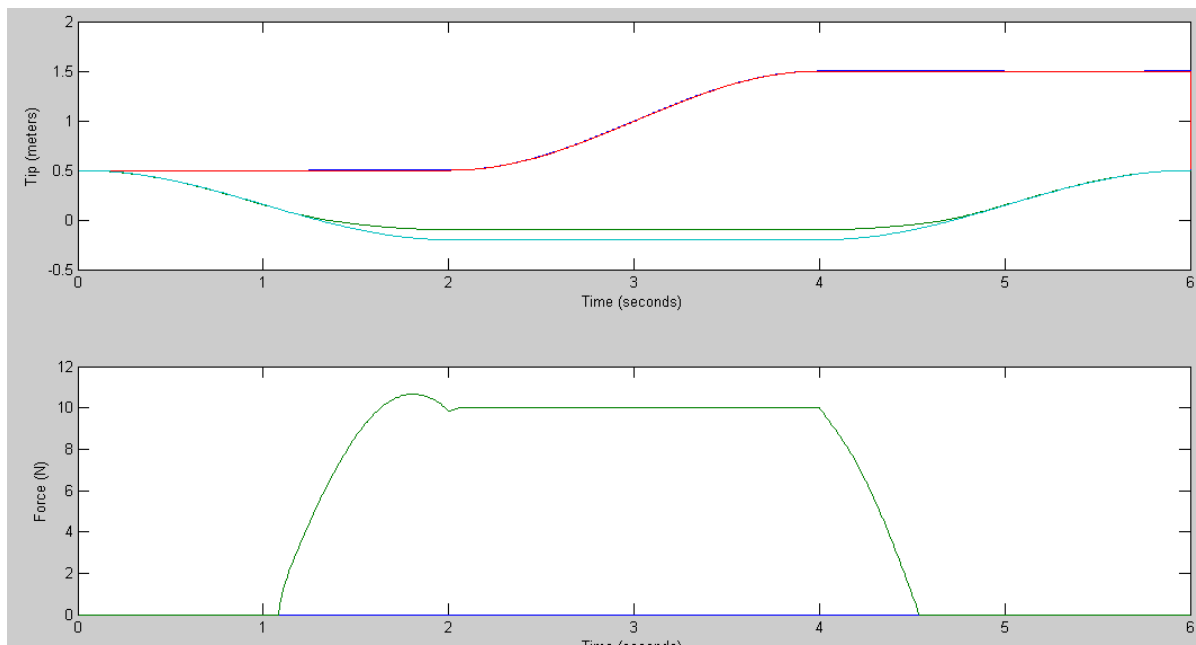
$$K_{net} = 100 || 100 = 50$$

for 10N of force, you need to try to move 0.2m into the floor

Simulation Results (XY_Floor_Control_v2.txt)



For a force of 10N, the desired position is 0.2m into the floor



Resulting tip position and tip force. When in contact with the floor, the force is 10N as desired.

Force Control (take 2)

While the former method works, it requires you to specify the path depending upon the chosen spring constant for the floor and the chosen P gain in the PID controller.

Using an integrator for force control works really well, however.

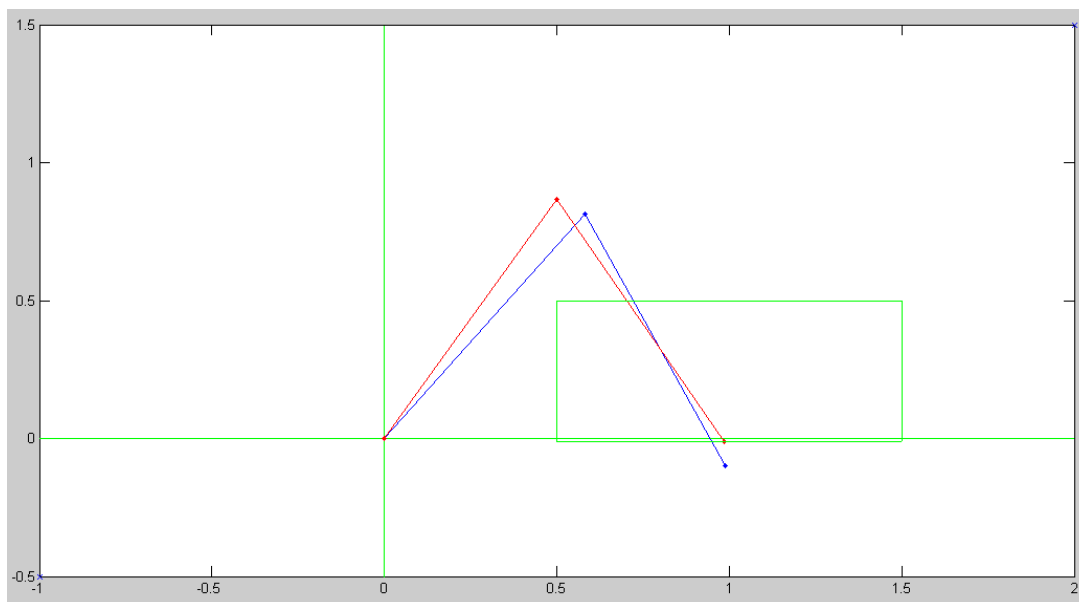
To get the best of both worlds, change the control law on the fly:

- When not in contact with the floor, use the PID position control law
- When you *are* in contact with the floor, use

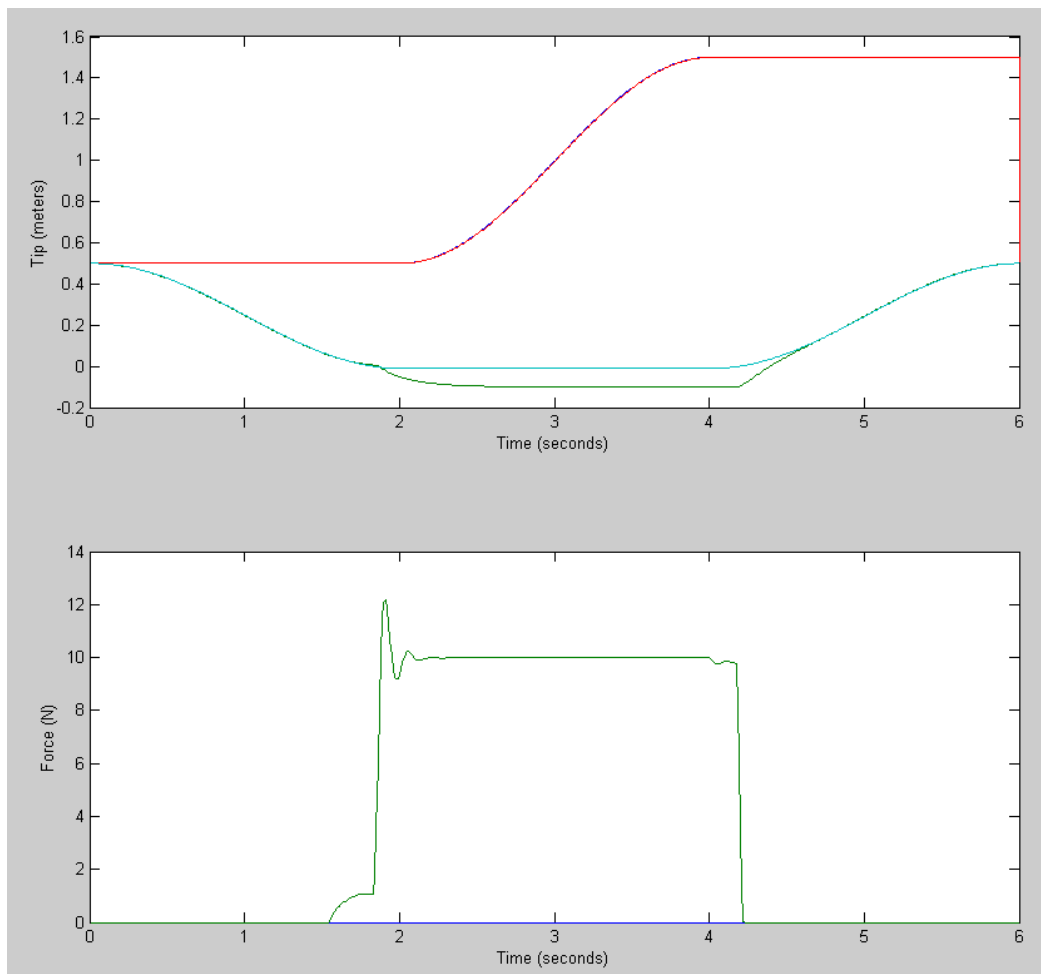
PID position control in the X direction

I force control in the Y direction

Simulation Results (RR_XY_Floor_Control_v3.txt)



Tracking Motion: $Y_{2ref} < 0$ so the robot is using force control



Resulting tip position and tip force. Note that while in contact the tip force is held at 10N as desired.

```

P0 = [0.5; 0.5];
P1 = [0.5; -0.01];
P2 = [1.5; -0.01];
P3 = [1.5; 0.5];
P4 = P0;

t = [0:0.01:1.99];
a = t/2;
a = (1 - cos(pi*a))/2;

% for a step change in poistion, add the following line
%a = 1*(a>0);

X1 = P0*(1-a) + P1*a;
X2 = P1*(1-a) + P2*a;
X3 = P2*(1-a) + P3*a;
X4 = P3*(1-a) + P4*a;
Xr = [X1, X2, X3, X4];
TIP = Xr;

% tip velocity ( used for feedforward control )
dXr = 0*Xr;
for i=2:length(Xr)-1
    dXr(:,i) = ( Xr(:,i+1) - Xr(:,i-1) ) / 0.02;
end

% tip acceleration (used for feedforward control )
ddXr = 0*Xr;
for i=2:length(Xr)-1
    ddXr(:,i) = ( dXr(:,i+1) - dXr(:,i-1) ) / 0.02;
end

Q = InverseRR( Xr(:,1) ) ;
dQ = [0; 0];
t = 0;
dt = 0.001;
Fy = 0;

% Start the simulation (dt = 0.001 for stability concerns)
Xq = [];
Tq = [];
Ff = [];

for i=1:length(Xr)
    Qr = InverseRR(Xr(:,i));
    for j=1:10
        X = [ cos(Q(1)) + cos(Q(1)+Q(2));
              sin(Q(1)) + sin(Q(1)+Q(2)) ];
        J = [ -(sin(Q(1)) + sin(Q(1)+Q(2))), -sin(Q(1)+Q(2)) ;
              (cos(Q(1)) + cos(Q(1)+Q(2))), cos(Q(1)+Q(2)) ];
        dX = J * dQ;

% Control Law and Feedforward Terms
        Facc = ddXr(:,i);
        Fpid = 100*(Xr(:,i) - X) + 20*(dXr(:,i) - dX );

% Floor ( spring with k = 100 )
        Ffloor = [ 0 ; 100*(0 - X(2)) + 20*(0 - dX(2)) ];
        Ffloor = max(0, Ffloor);
    end
end

```

```

% Control the force to 10N if Y2r < 0
    if (Xr(2,i) < 0)
        dFy = 100*(10 - Ffloor(2));
        Fy = Fy + dFy*dt;
    else
        Fy = 0;
    end

% gravity
    Tg = -9.8 * [ 2*cos(Q(1)) + cos(Q(1) + Q(2)); cos(Q(1) + Q(2)) ];

    T = (J') * ( Fpid + Facc + Ffloor - [ 0 ; Fy ] ) - Tg;

    ddQ = RRDynamics(Q, dQ, T);
    dQ = dQ + ddQ * dt;
    Q = Q + dQ*dt;
    t = t + dt;
end

RR(Q, Qr, TIP);

Xq = [Xq, X];
Tq = [Tq, T];
Ff = [Ff, Ffloor];
end

t = [1:length(Xr)] * 0.01;
t = min(t,6);
clf
subplot(211)
plot(t,Xq,t,Xr);
xlabel('Time (seconds)');
ylabel('Tip (meters)');
subplot(212)
plot(t,Ff);
xlabel('Time (seconds)');
ylabel('Force (N)');

```